

# **DLR Contribution to the 2nd High Lift Prediction Workshop**

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**DLR, German Aerospace Center**

**Institute of Aerodynamics and Flow Technology, Braunschweig**



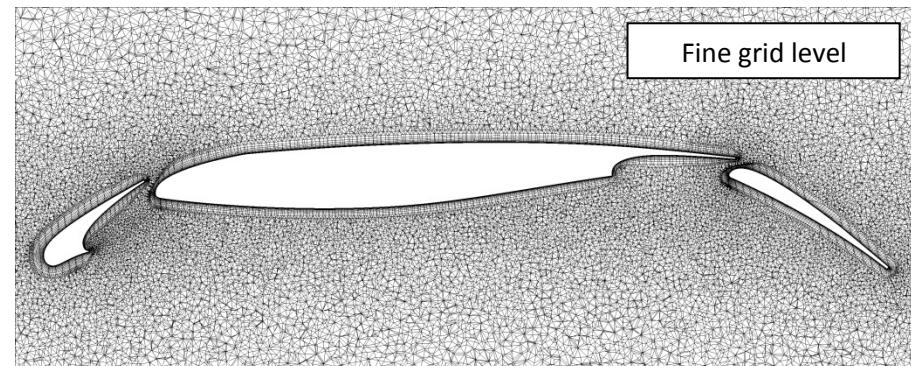
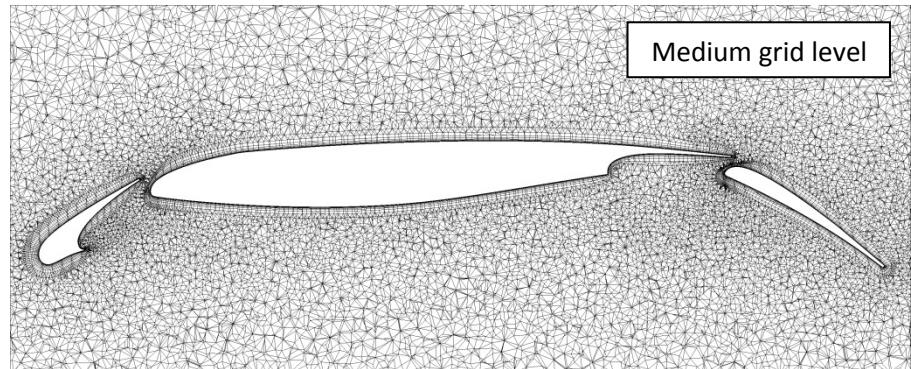
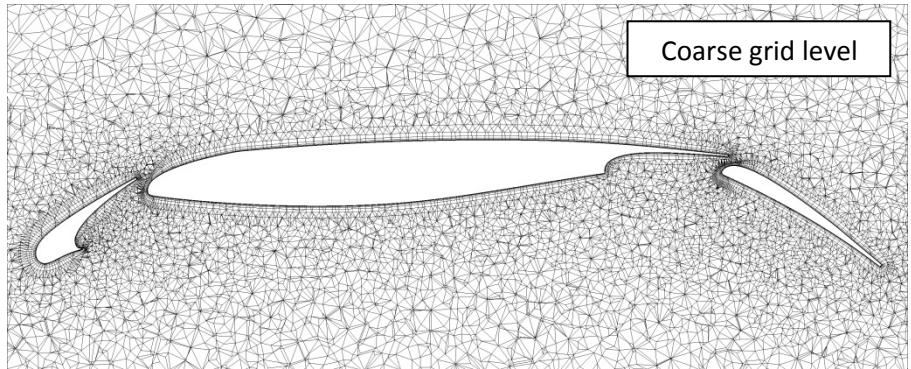
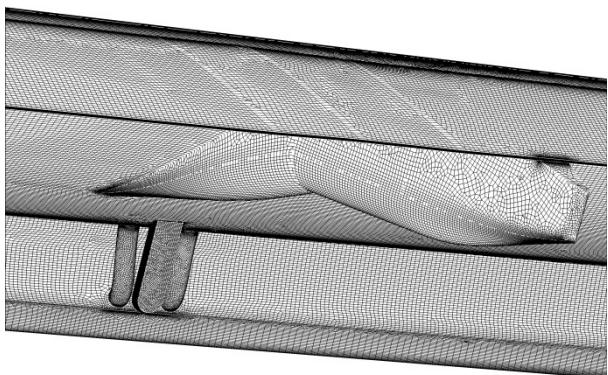
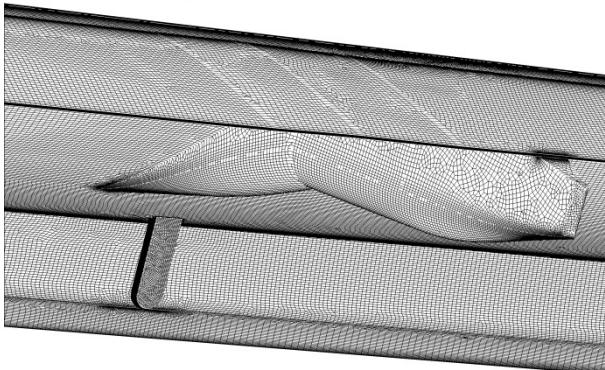
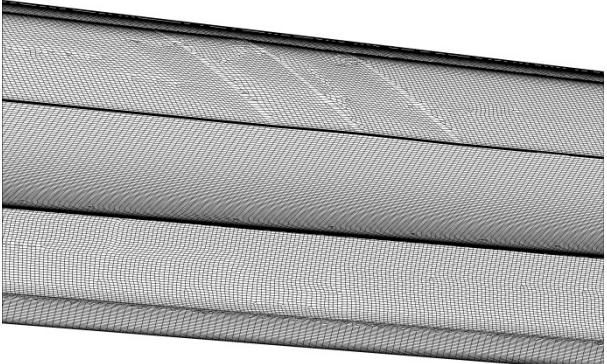
**Knowledge for Tomorrow**

- DLR Contribution and Objectives for HiLiftPW-2 Computations
- SOLAR grids and TAU-solver settings
- Baseline validation based on (Case 3a)
- Reynolds Number Effects (Case 3a - Case 3b)
- Impact of Wind tunnel Model Details (Case 3b - Case 2b - Case1)
- Impact of Pressure Tube Bundles, Validation (Case2a - Case3a)
- Turbulence Model Variation SA-RC (Case3a)
- Grid Refinement Study
- Conclusion and Outlook

- **Grid Generation: Supply of hybrid unstructured grids for all Configurations based on SOLAR grid generation system**
  - Assessment of present SOLAR features taking into account grid family requirement and gridding guidelines (a.f.a.p.)
  - Grid refinement study for moderately complex 3D configuration variations
  - Reynolds number adapted gridding approach
- **Numerical analysis based on TAU computations**
  - Improved understanding of geometry simplifications at low and high Re-No. conditions and scaling effects
  - Assessment of TAU capability to simulate OoM Reynolds-number effects
  - Improved understanding of simulation quality and shortcomings
  - Turbulence model performance assessment
  - Identification of grid resolution and topology impact

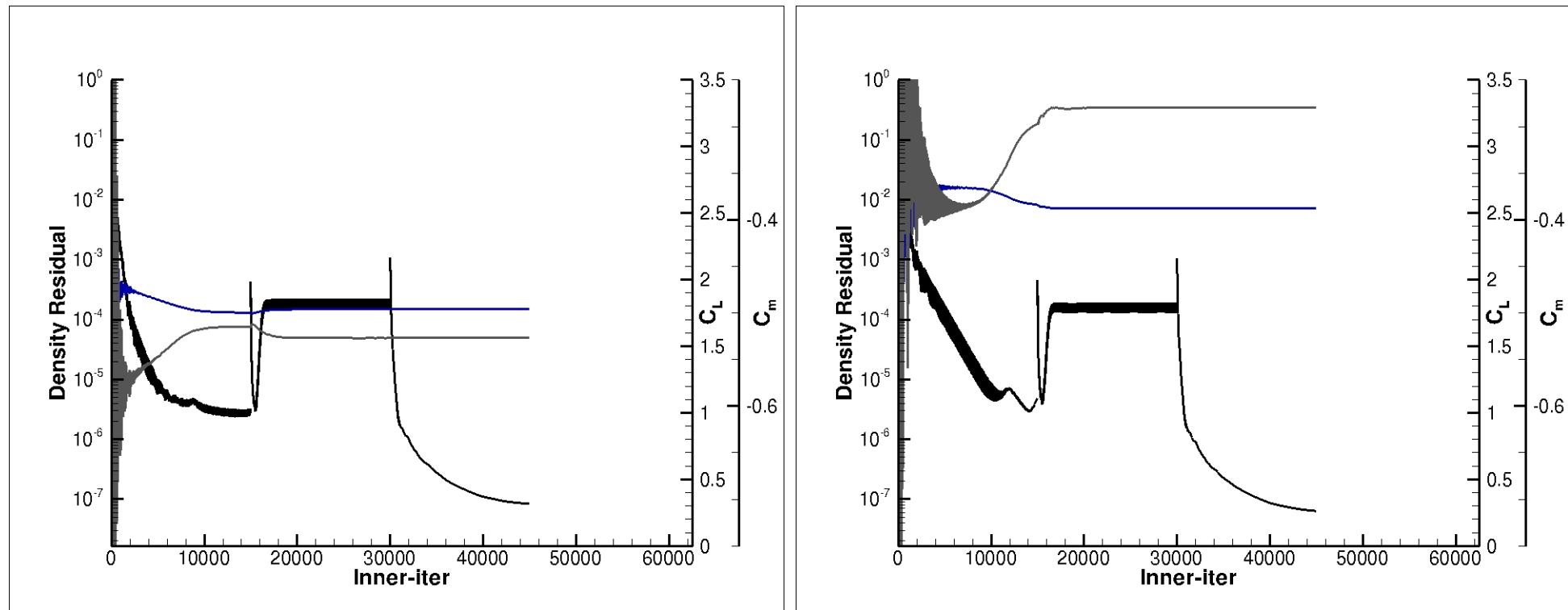
- Hybrid unstructured grids, hex-based near surfaces, individual grids for all configurations and Reynolds number conditions
- Grid generation and adaptation approach
  - $y^+$  -manual adaptation, const. first cell height
  - grid family approach according to DPW IV, HiLiftPW-1 (SOLAR)
  - special treatment of sources
- Grids provided for low Re conditions for complexity stages II, IV and V
  - total grid point numbers: 29.7 mil. / 37.3 mil / 37.7 mil.
- Grids provided for high Re conditions for complexity stages II, IV and V
  - total grid point numbers: 25.6 mil. / 32.4 mil / 34.2 mil.
- Grid family for Stage II, (high Re) with 3 levels
  - total grid point numbers: 9.2 mil. / 25.6 mil / 73.4 mil.

- Characteristics of the DLR-SOLAR grids



- **Code Version:** DLR TAU code 2012.1.0
- **Spatial Discretization:**
  - **Main equations:** Jameson central, 2<sup>nd</sup> order;  
Blend scalar (20%) – matrix (80%) dissipation
  - **Turbulent equations:** AUSMDV upwind, 2<sup>nd</sup> order
  - **Full NS Discretization**
- **Turbulence Models:**
  - Spalart-Allmaras, original 1992 formul. (SAO)
  - Spalart-Allmaras with rotational correction (SARC)
- **Temp. Integration:**
  - LU-SGS Backward Euler
  - Multigrid, 3V cycle, main and turb. equations
  - final set of iterations approaching global time step

- Convergence of main flow residual, density, lift, and moment for  $\alpha = 7^\circ$  and  $\alpha = 18.5^\circ$



## Case 3a

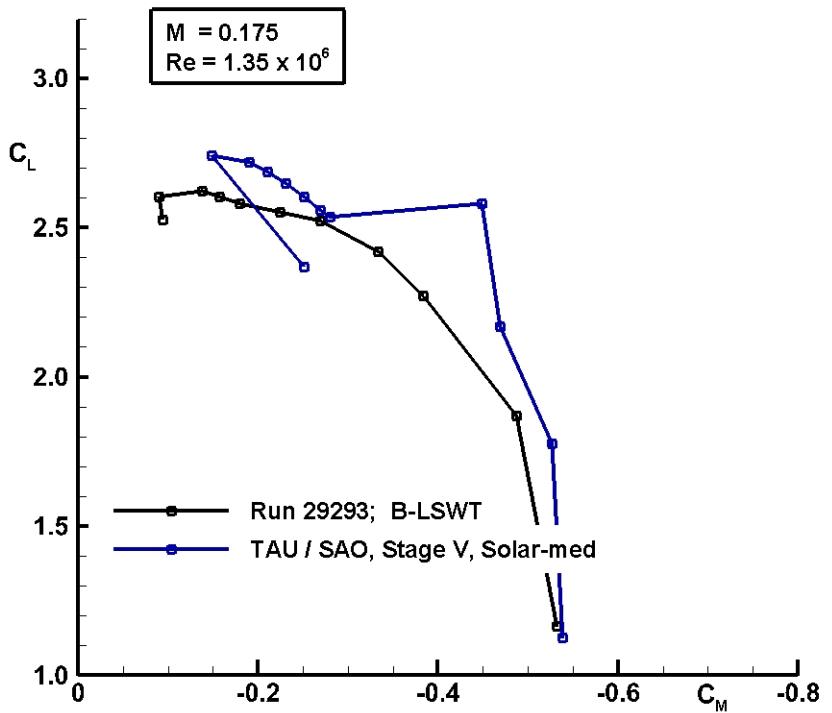
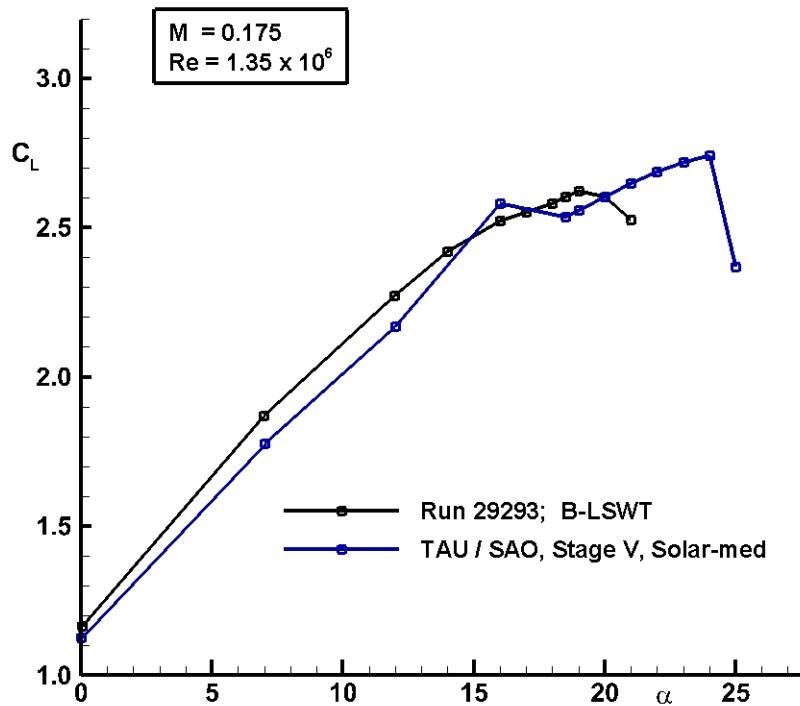
**TAU-SAO / SOLAR**

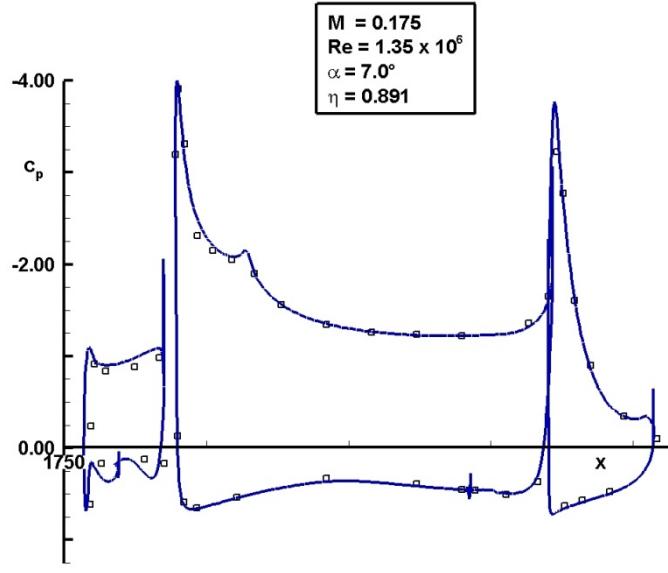
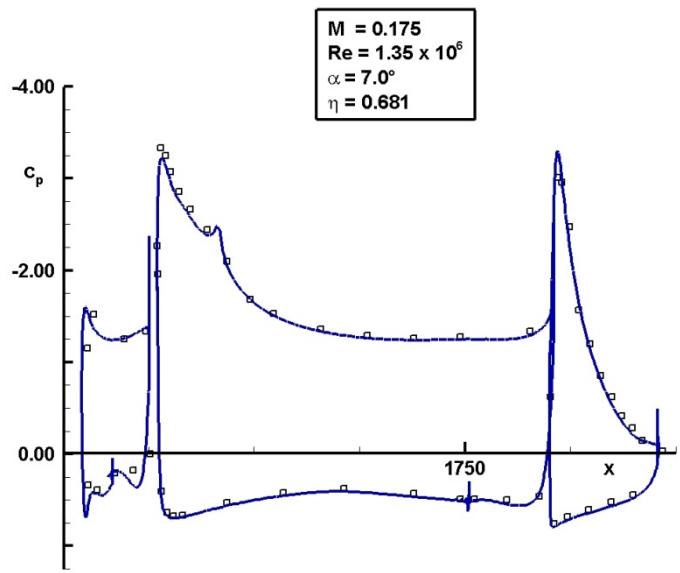
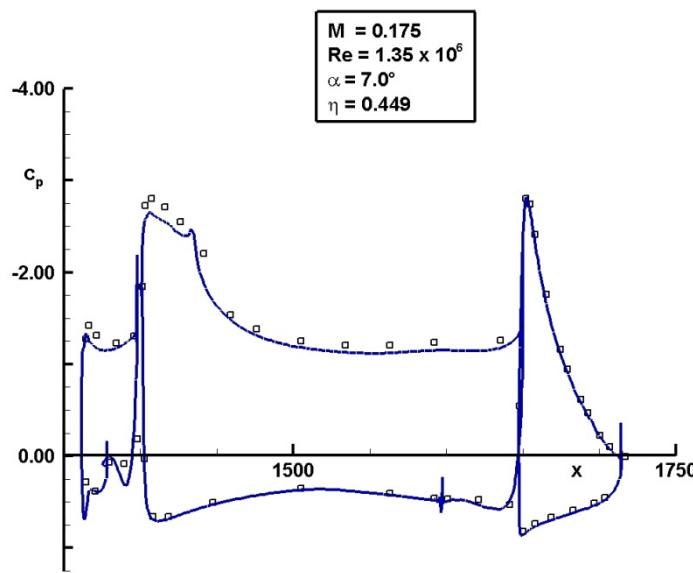
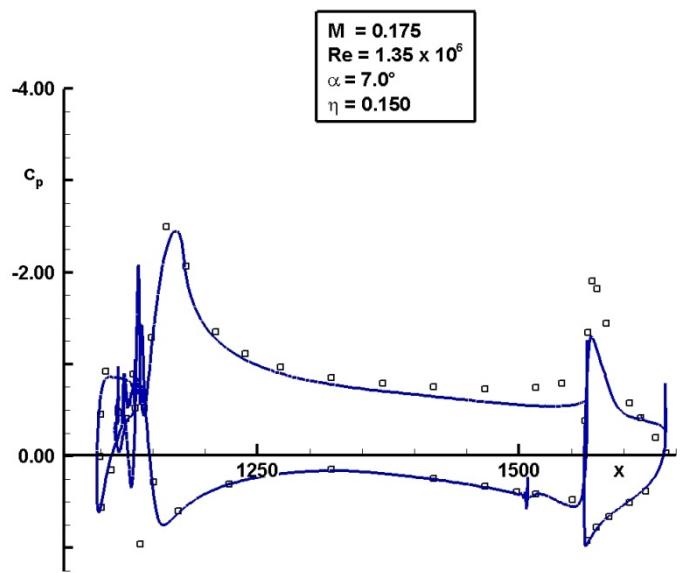
**Baseline Validation**

**Full Complexity (WB+HLS+PFS+FTF+ST+PTB)**

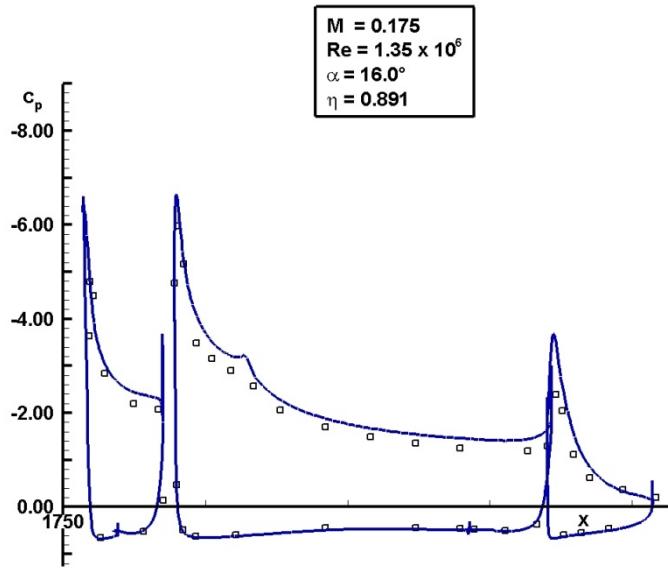
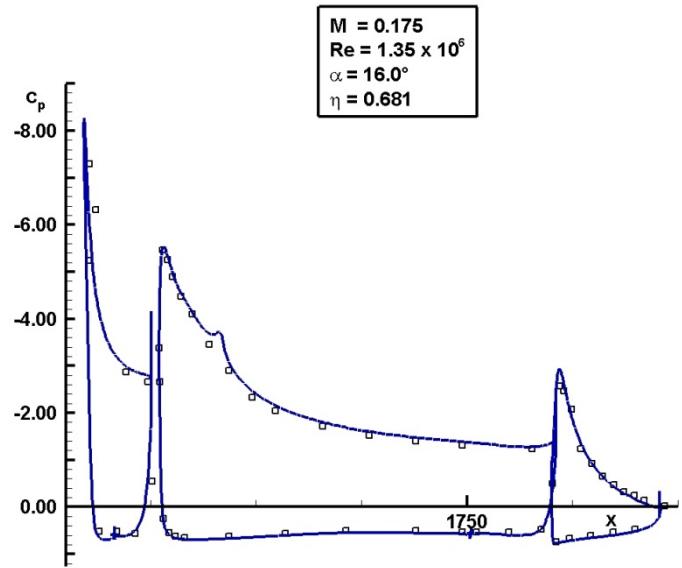
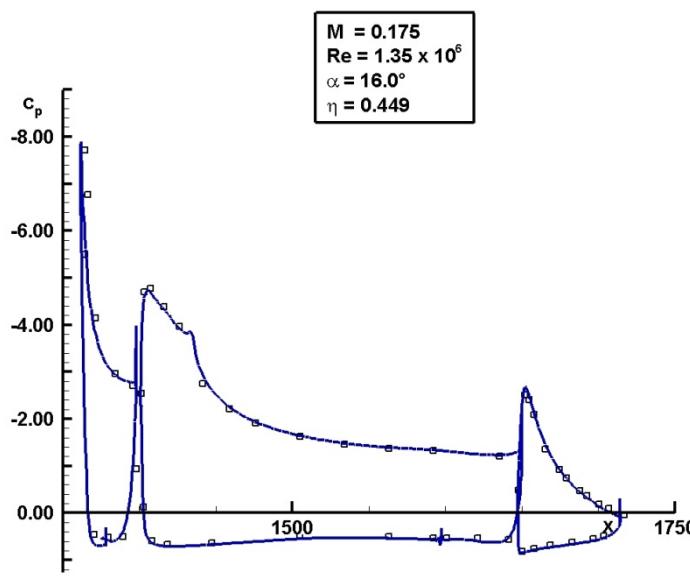
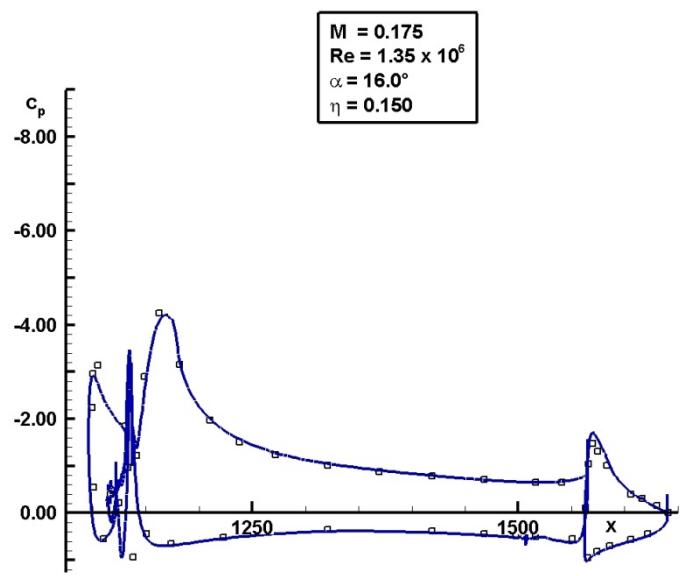
**Low Re No.**

- Lift curve and pitching moment

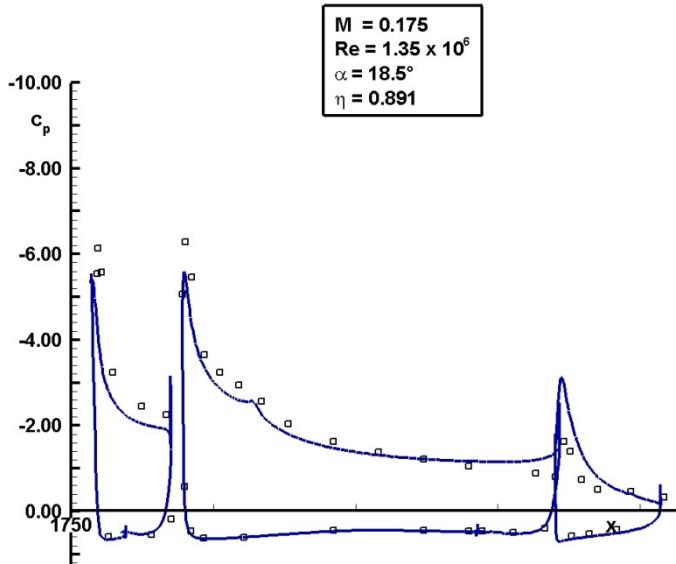
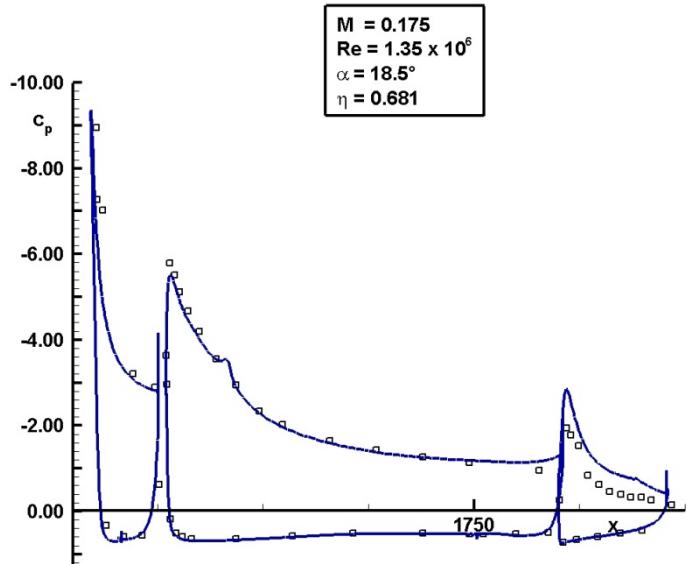
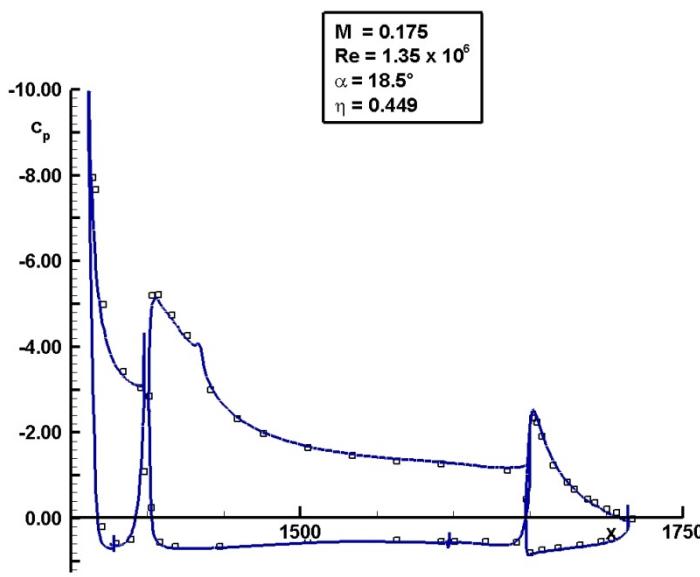
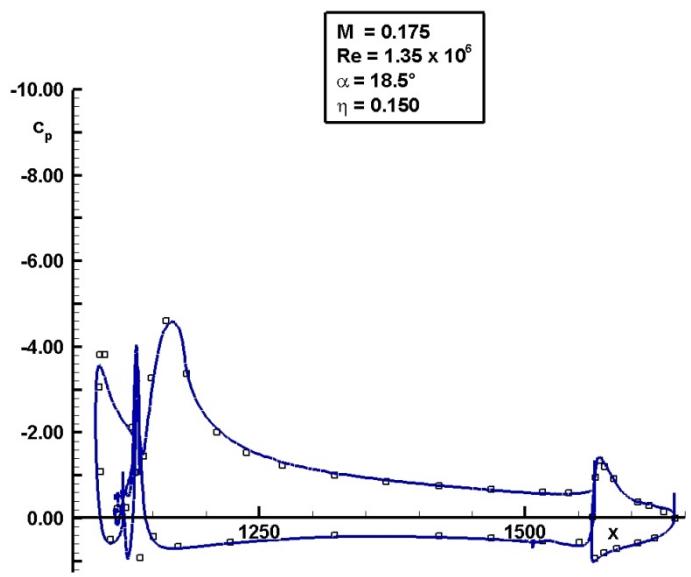




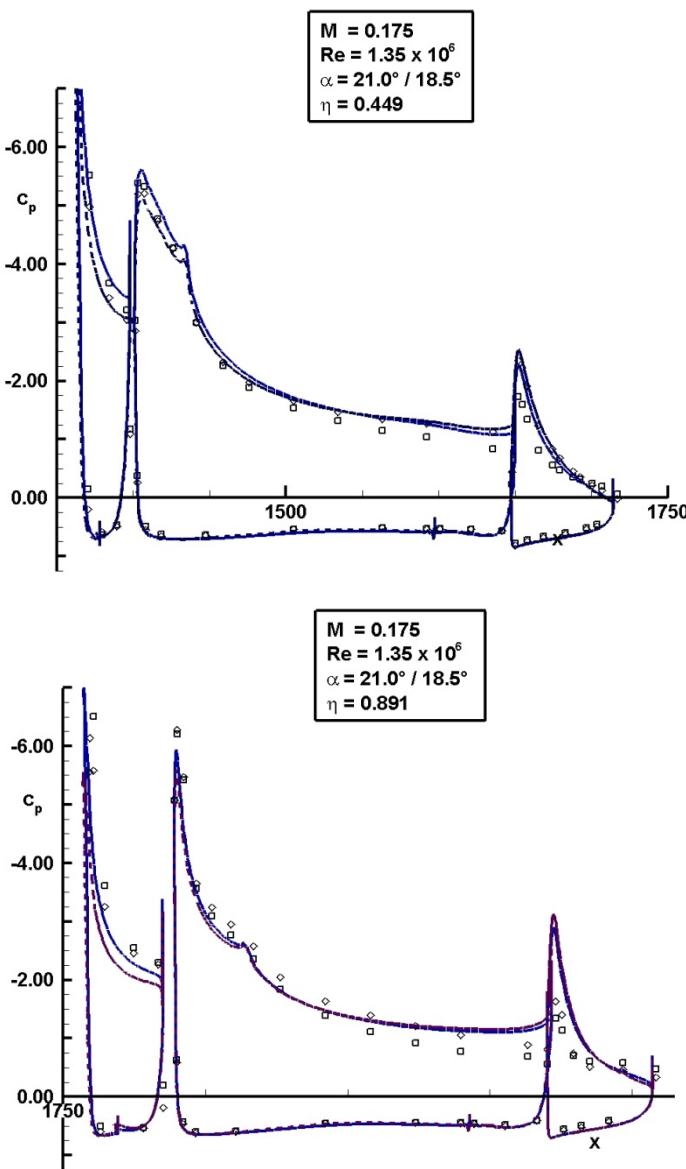
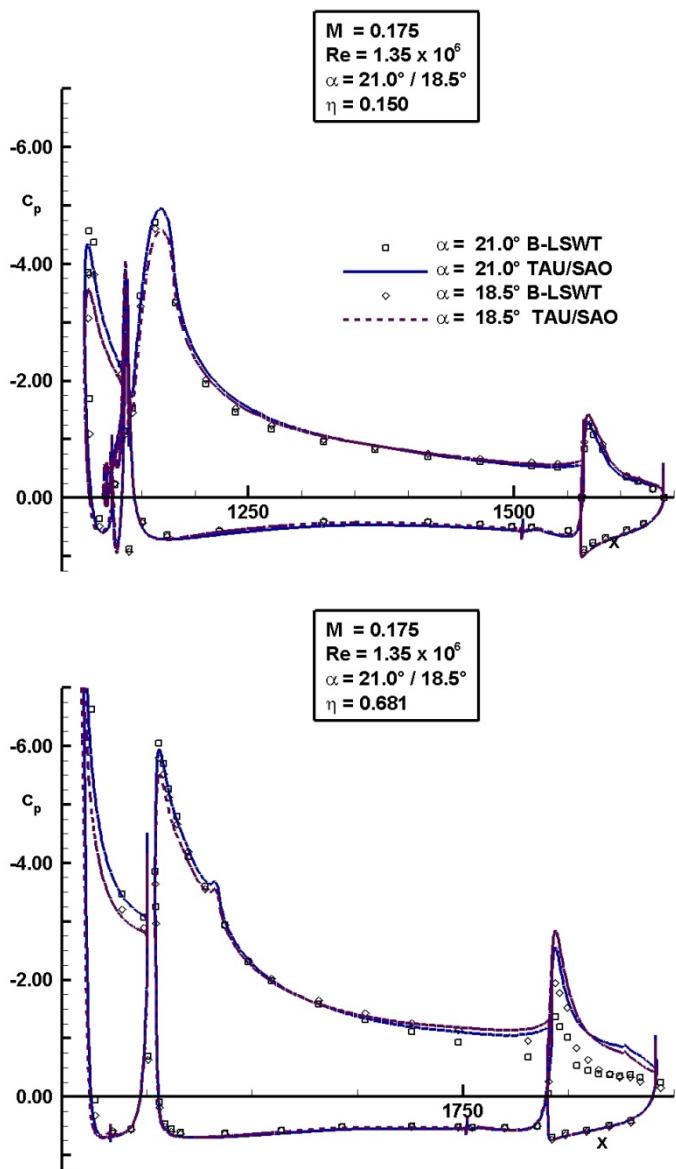
$\alpha = 7^\circ$   
**PS1, PS4,  
 PS6, PS10**



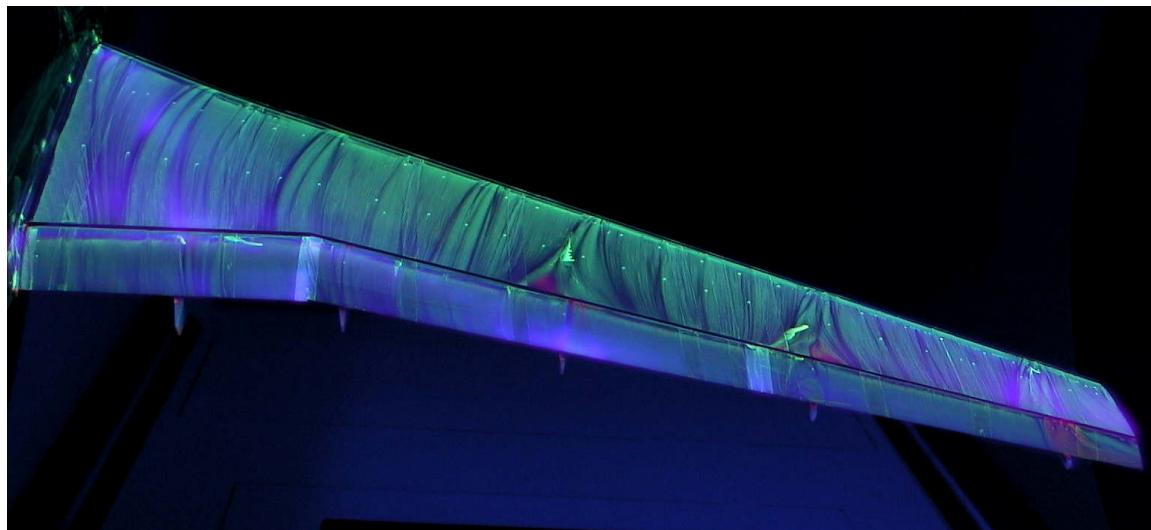
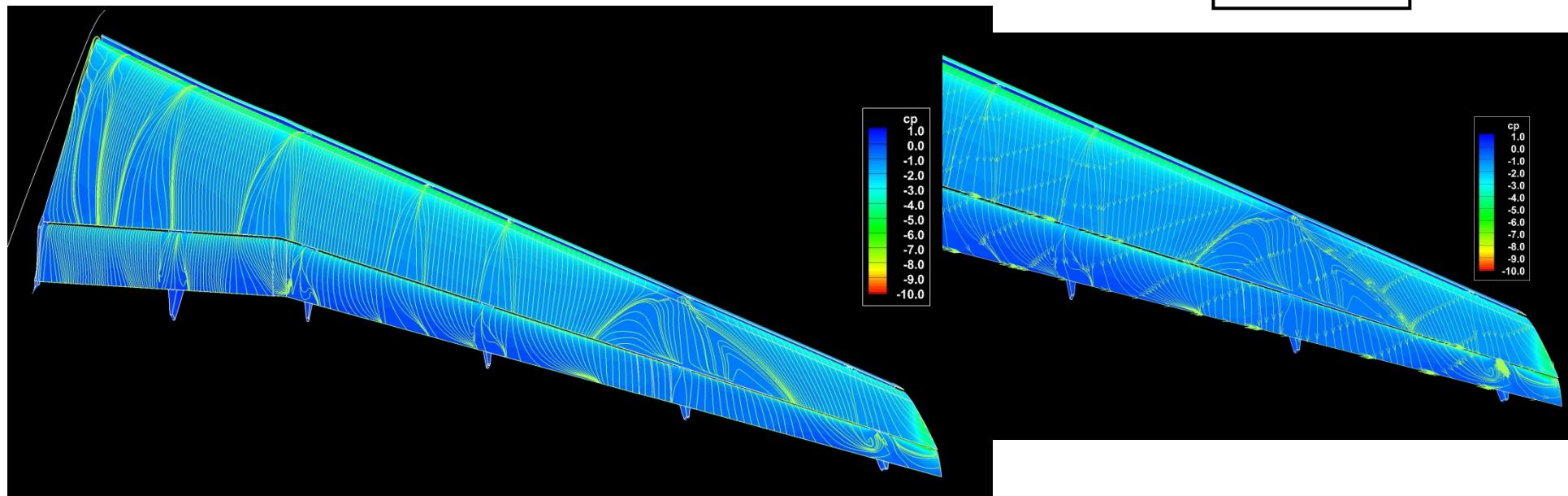
**$\alpha = 16^\circ$**   
**PS1, PS4,**  
**PS6, PS10**



**$\alpha = 18.5^\circ$**   
**PS1, PS4,**  
**PS6, PS10**



**$\alpha = 21^\circ$**   
**PS1, PS4,**  
**PS6, PS10**

 $\alpha = 18.5^\circ$ 

## **Case 3b ( vs. Case3 a)**

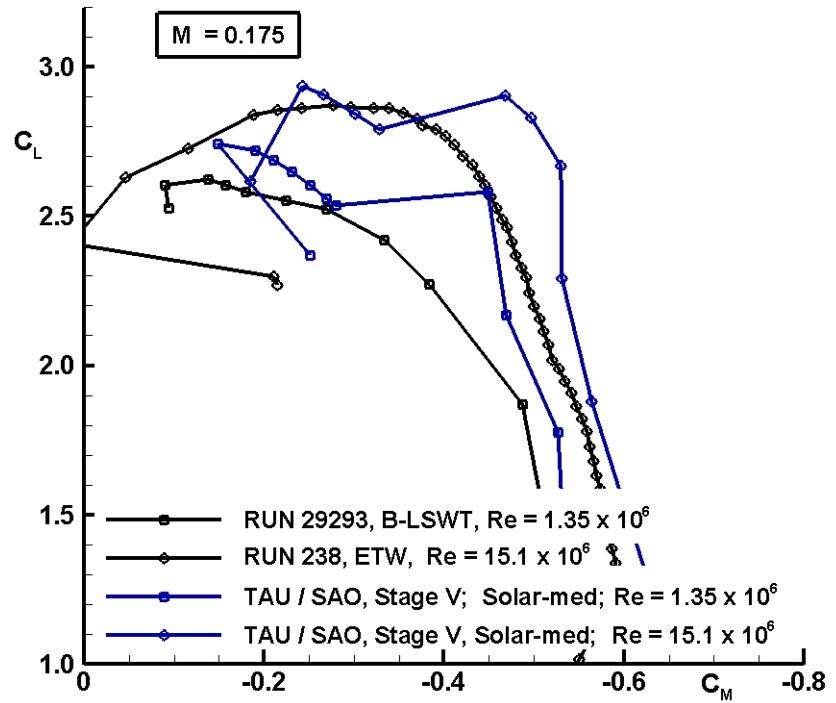
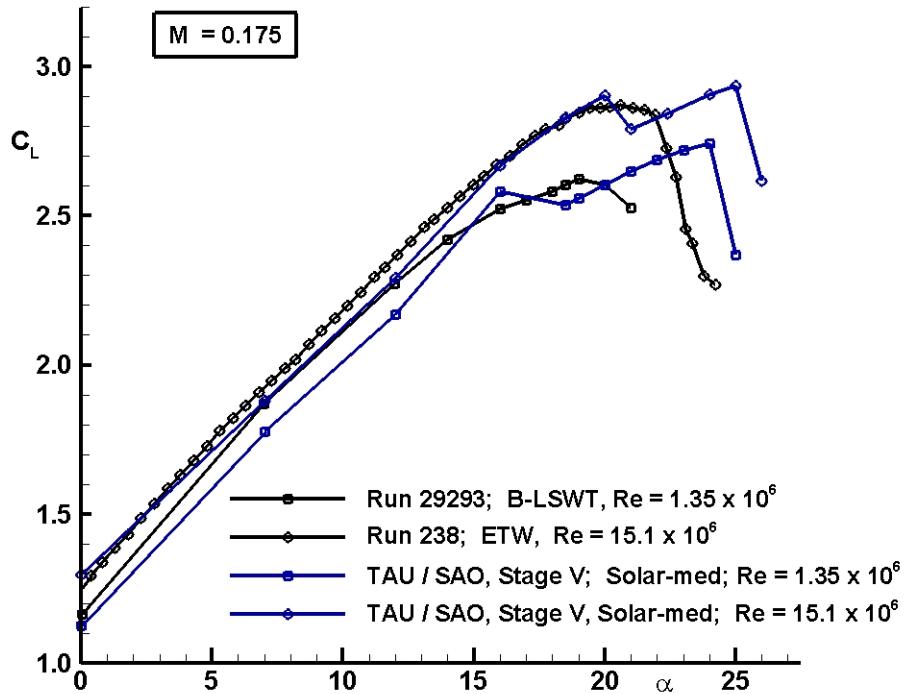
**TAU-SAO / SOLAR**

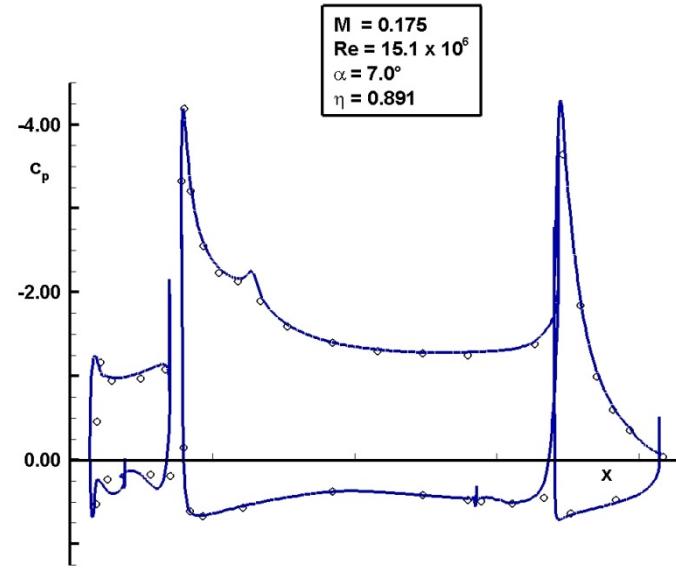
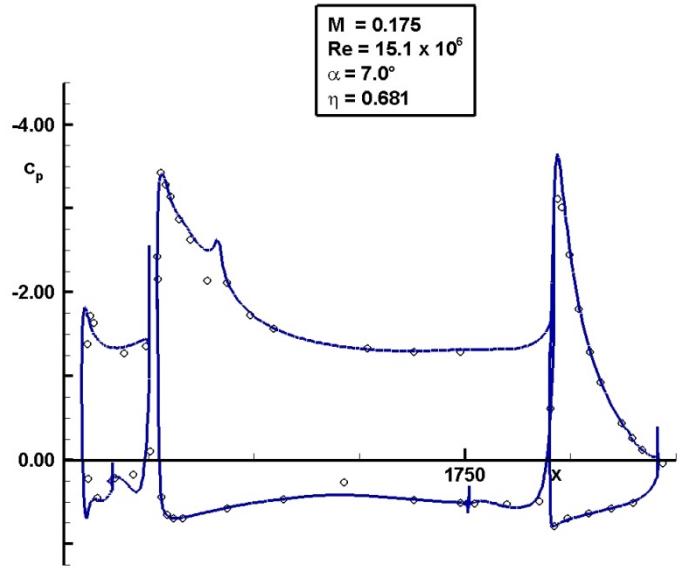
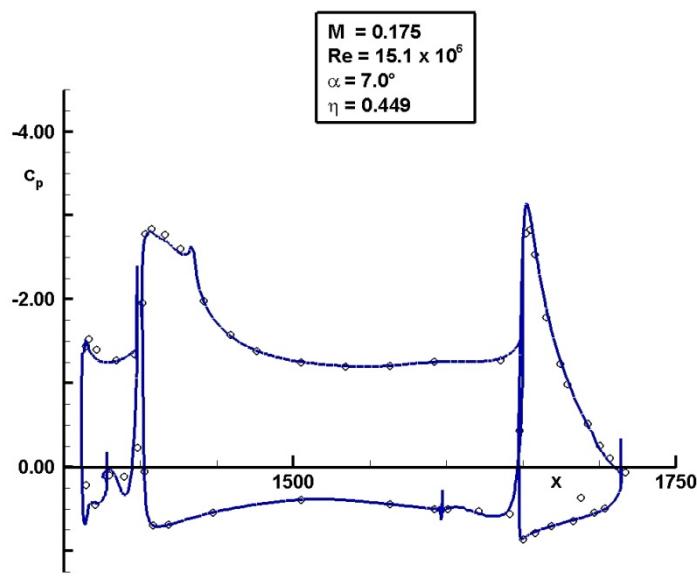
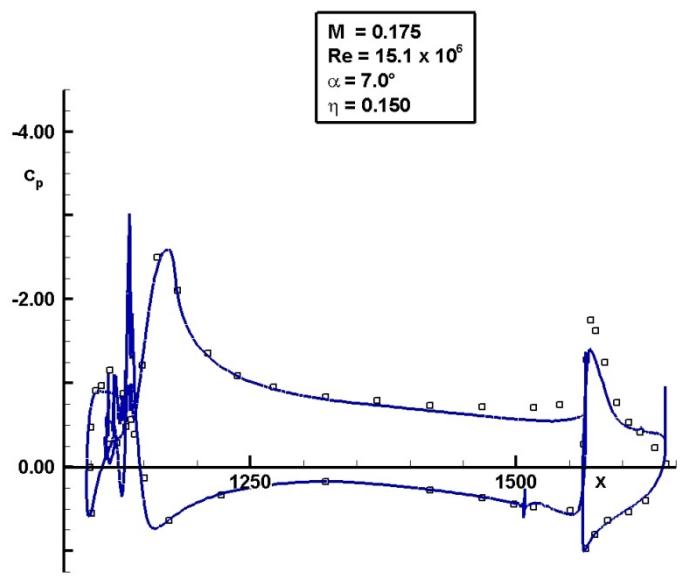
**Reynolds Number Effects**

**Full Complexity (i.e. WB+HLS+PFS+FTF+ST+PTB)**

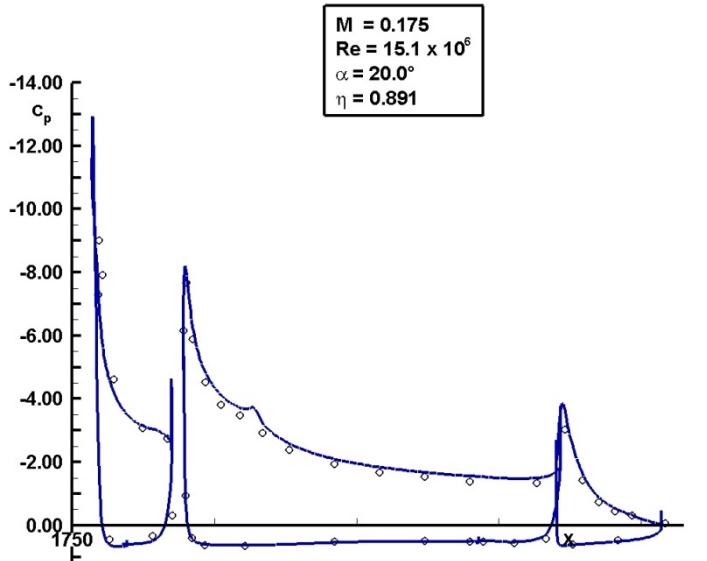
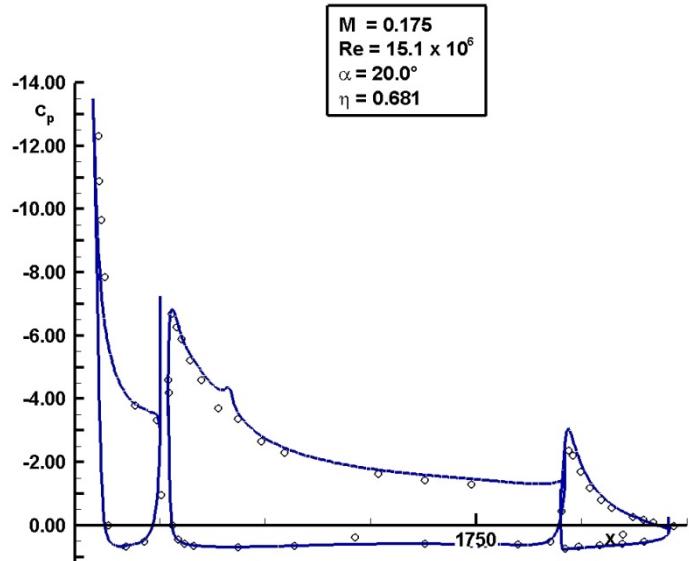
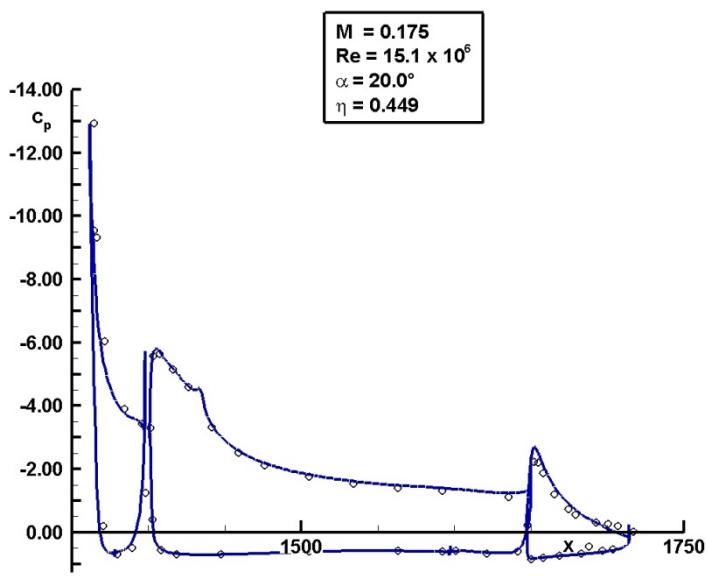
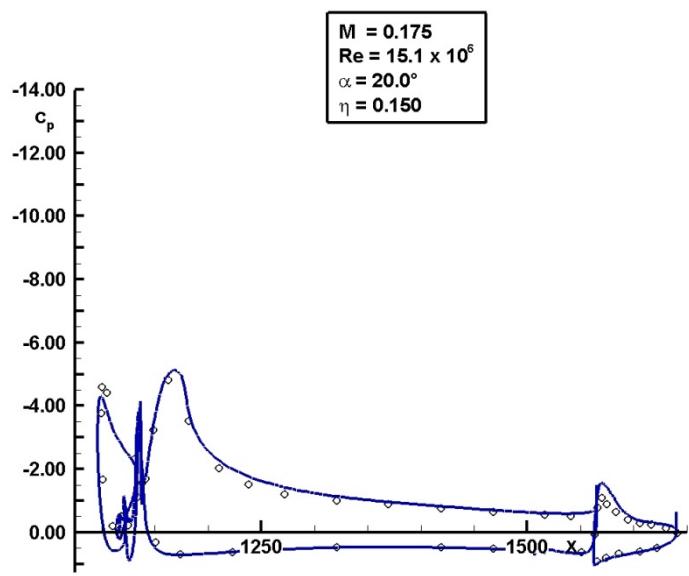
**High Re No.**

- Lift curve and pitching moments 3a vs. Case 3b

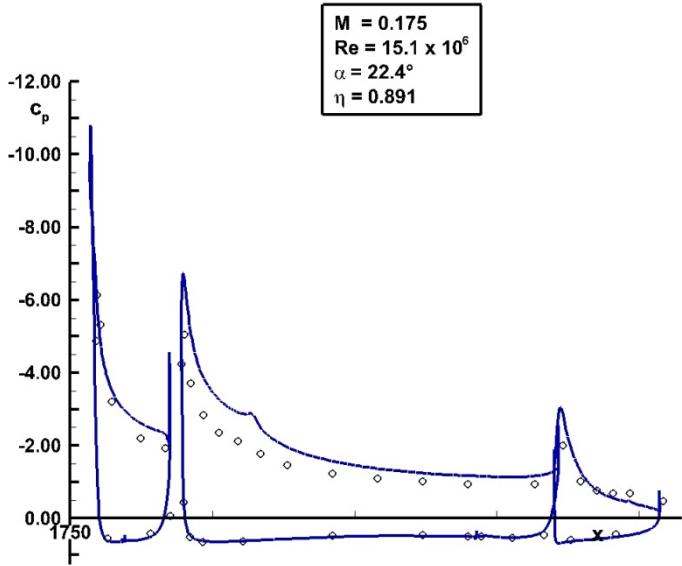
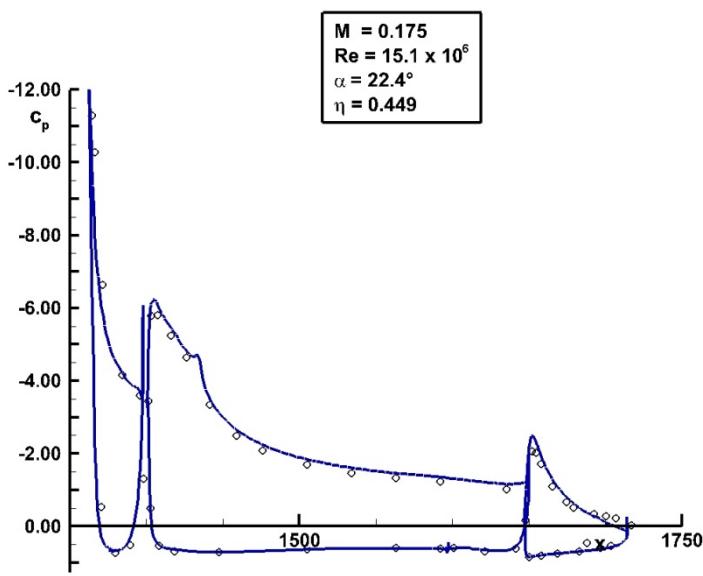
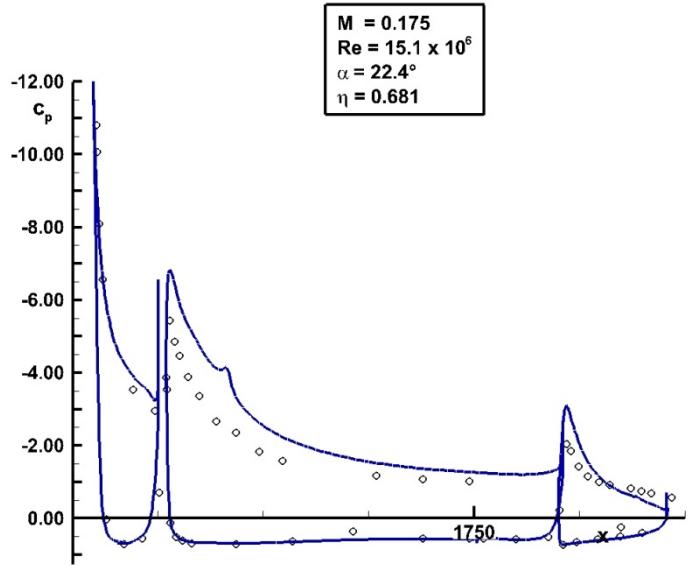
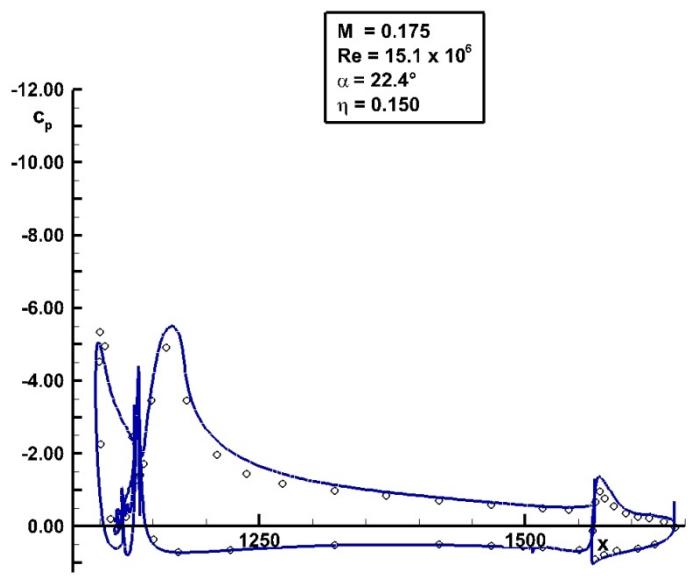




$\alpha = 7^\circ$   
**PS1, PS4,  
 PS6, PS10**



**$\alpha = 20^\circ$**   
**PS1, PS4,**  
**PS6, PS10**



$\alpha = 22.4^\circ$   
**PS1, PS4,  
 PS6, PS10**

## Case 3b vs. Case 2b vs. Case 1

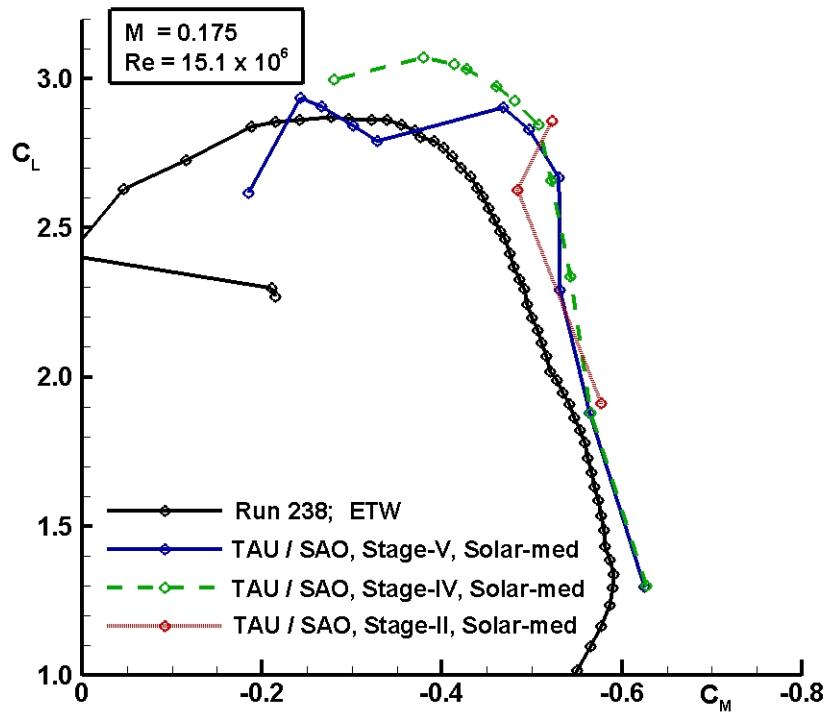
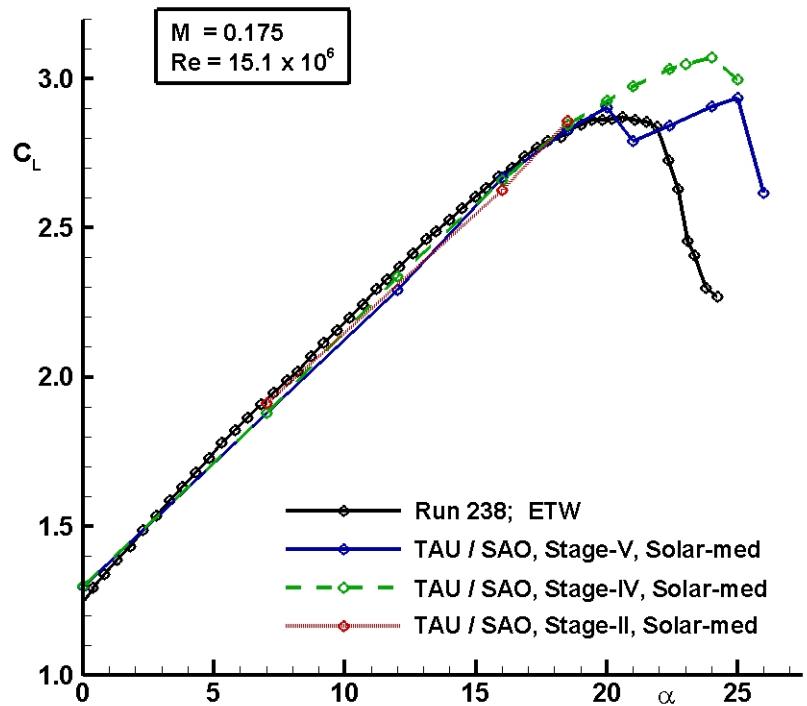
TAU-SAO / SOLAR

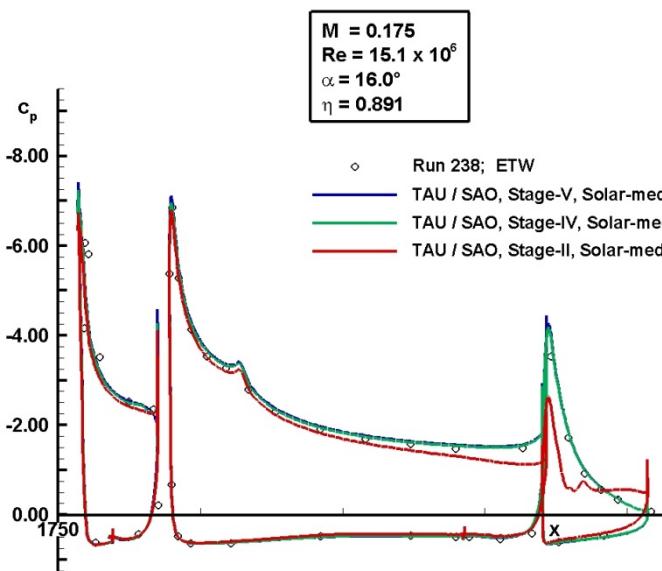
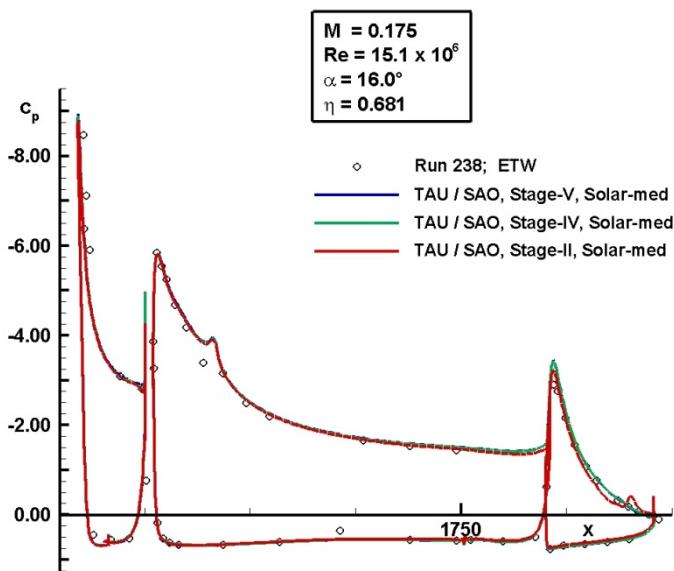
Impact of Wind Tunnel Model Details

Varying Complexity

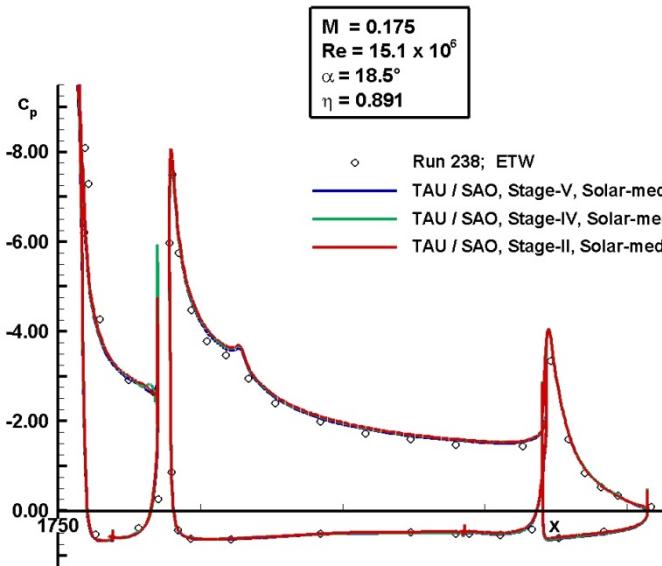
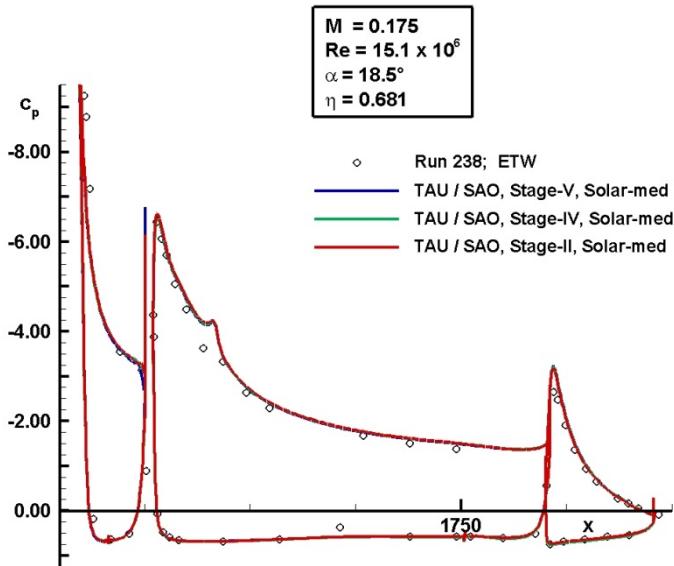
High Re No.

- Lift curve and pitching moment

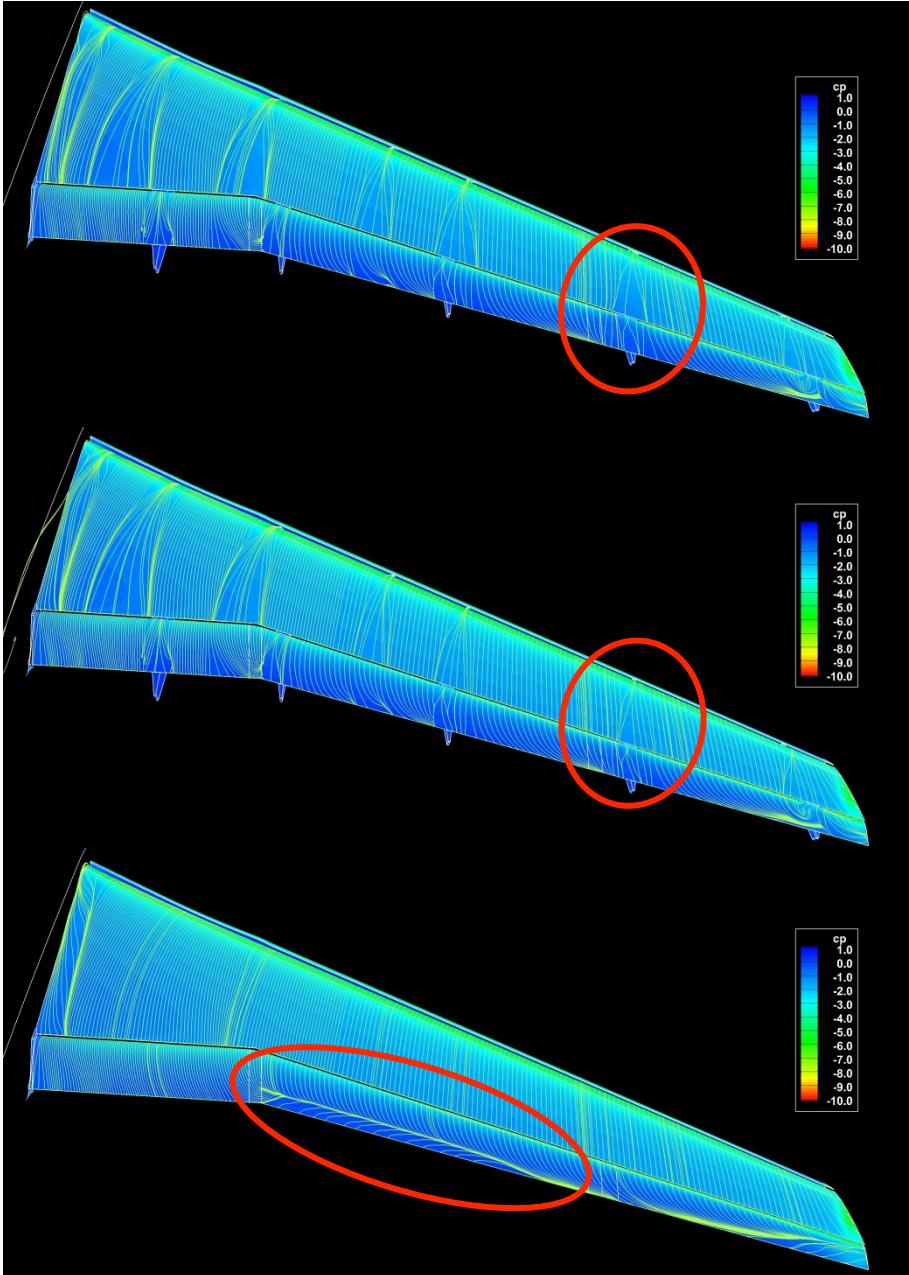




$\alpha = 16.0^\circ$   
**PS6, PS10**



$\alpha = 18.5^\circ$   
**PS6, PS10**

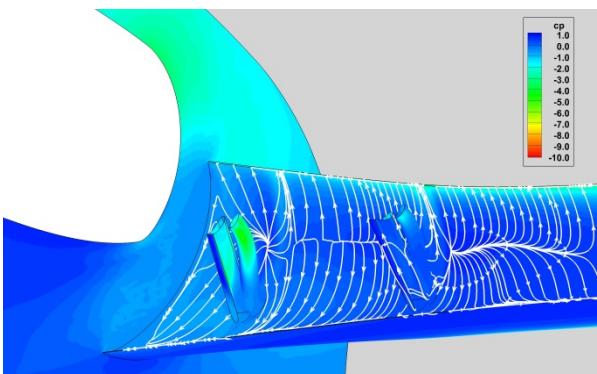
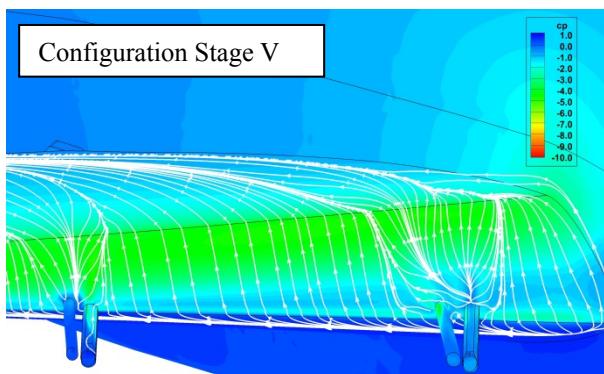
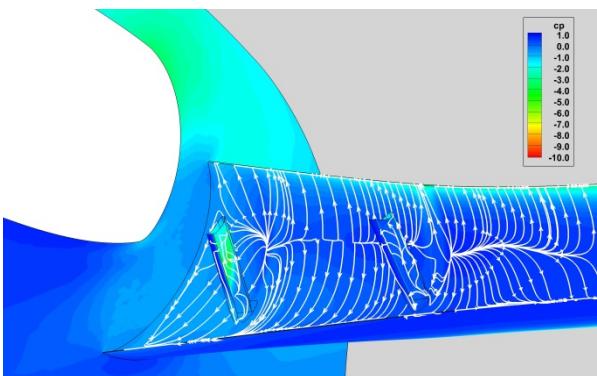
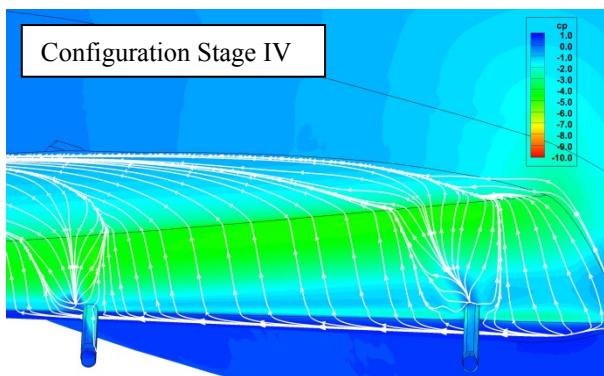
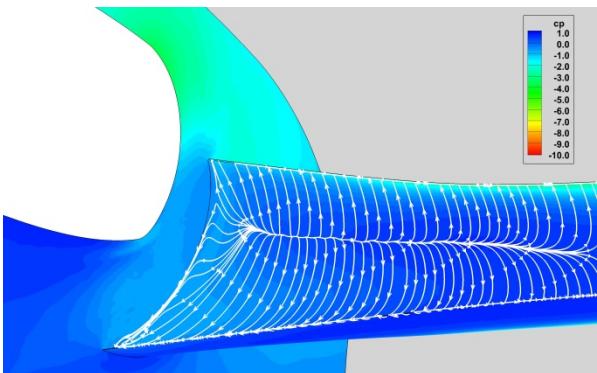
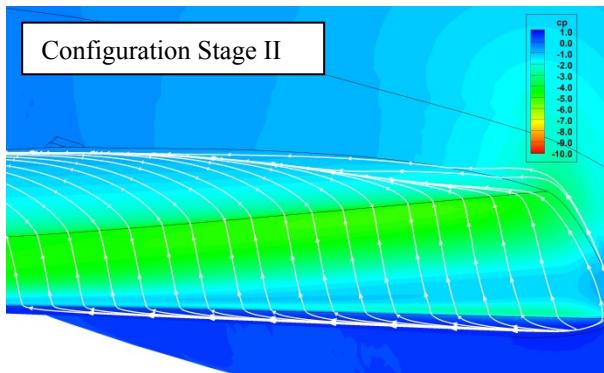


Case 3b, Configuration Stage V

$\alpha = 18.5^\circ$

Case 2b, Configuration Stage IV

Case 1, Configuration Stage II



$\alpha = 18.5^\circ$

## Case 3a vs. Case 2a

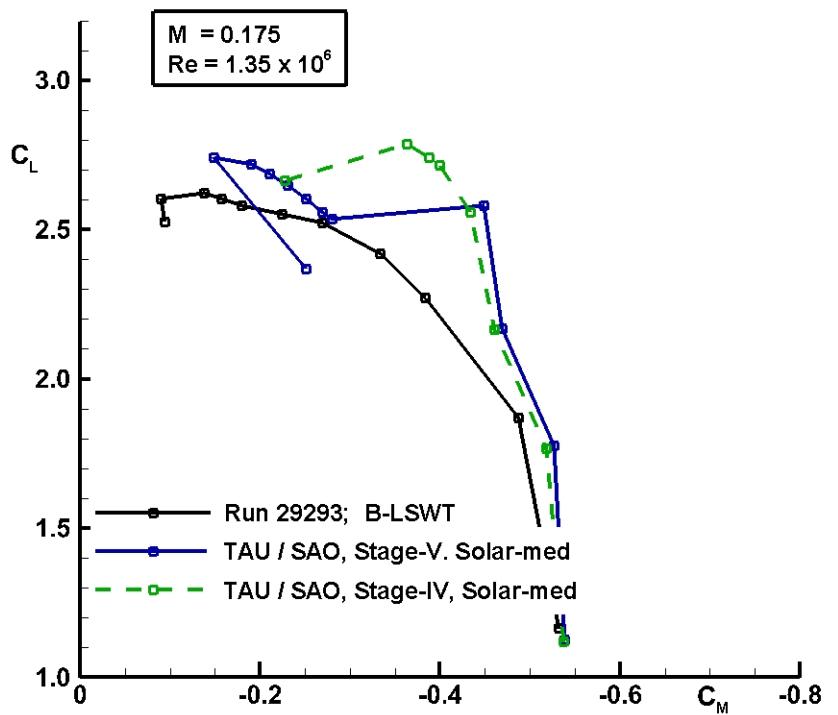
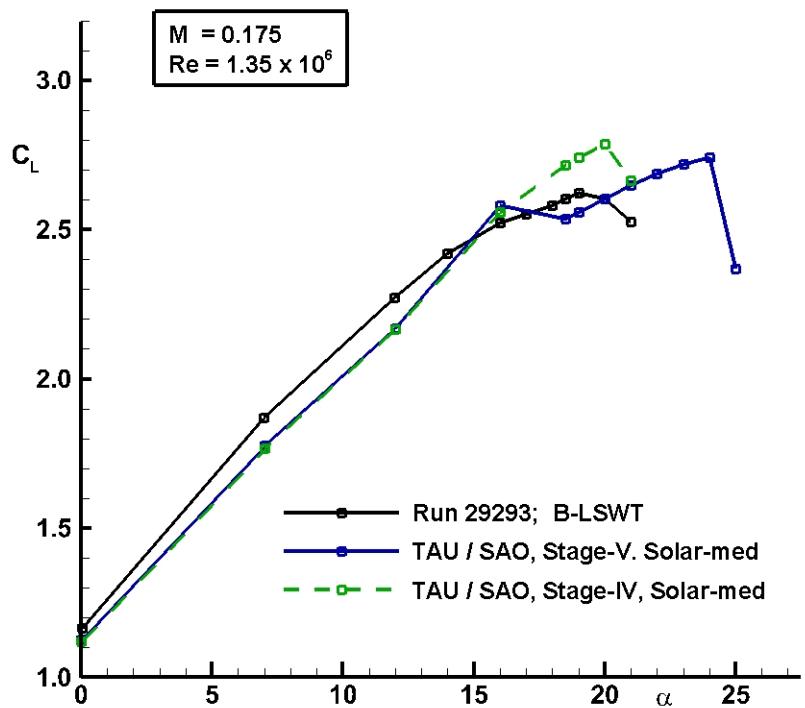
TAU-SAO / SOLAR

**Impact of Pressure Tube Bundles, Validation**

**Varying Complexity (+/- PTB)**

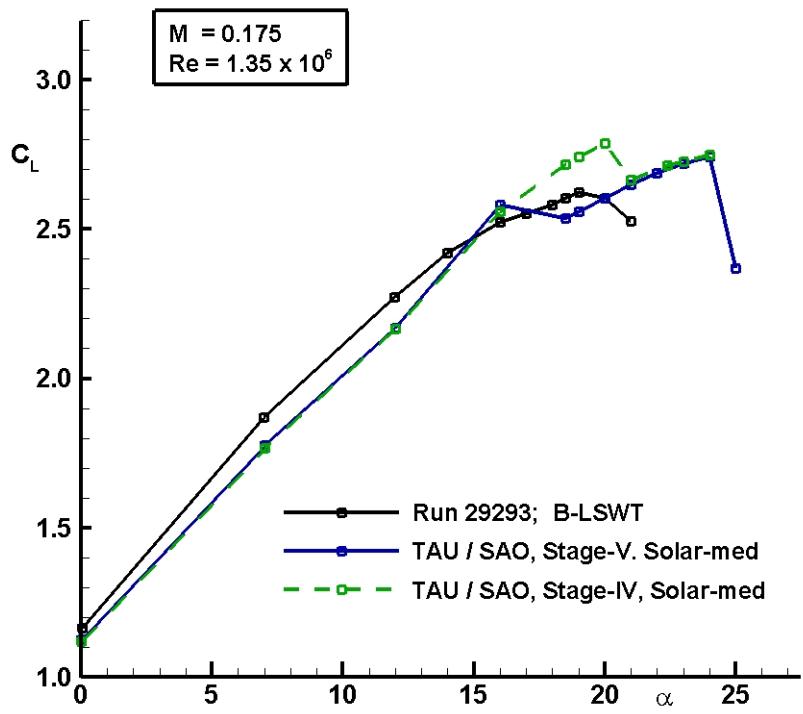
**Low Re No.**

- Lift curve and pitching moment

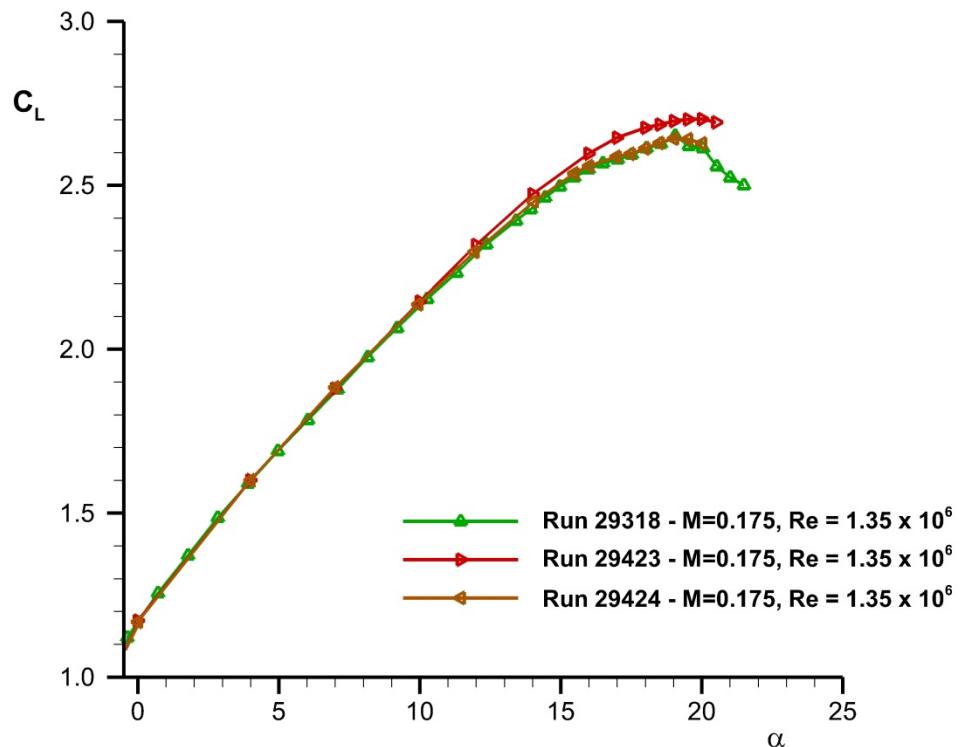


- Lift curves

Computations TAU-SAO



B-LSTW W/T Experiment



## Case 3a

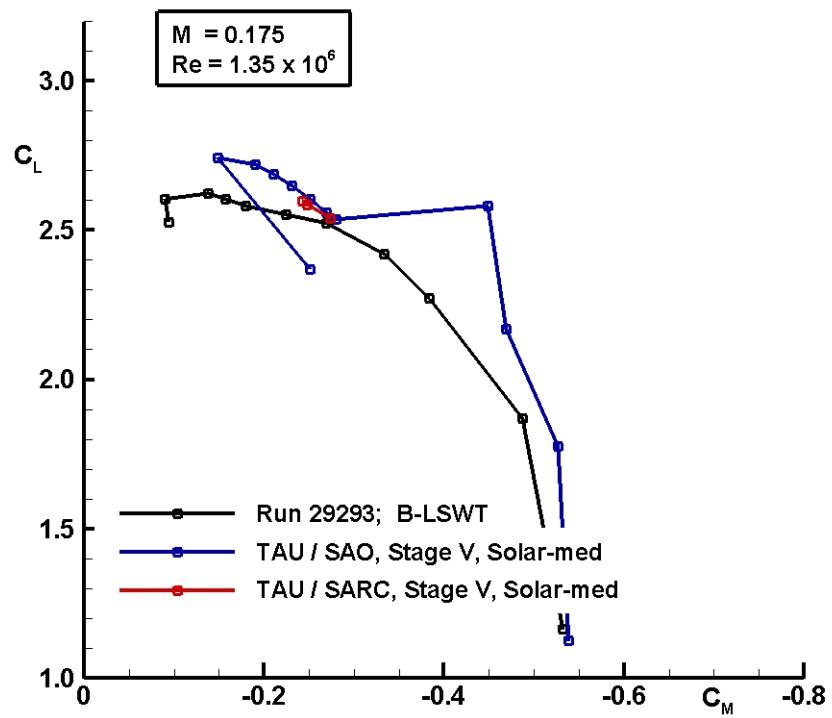
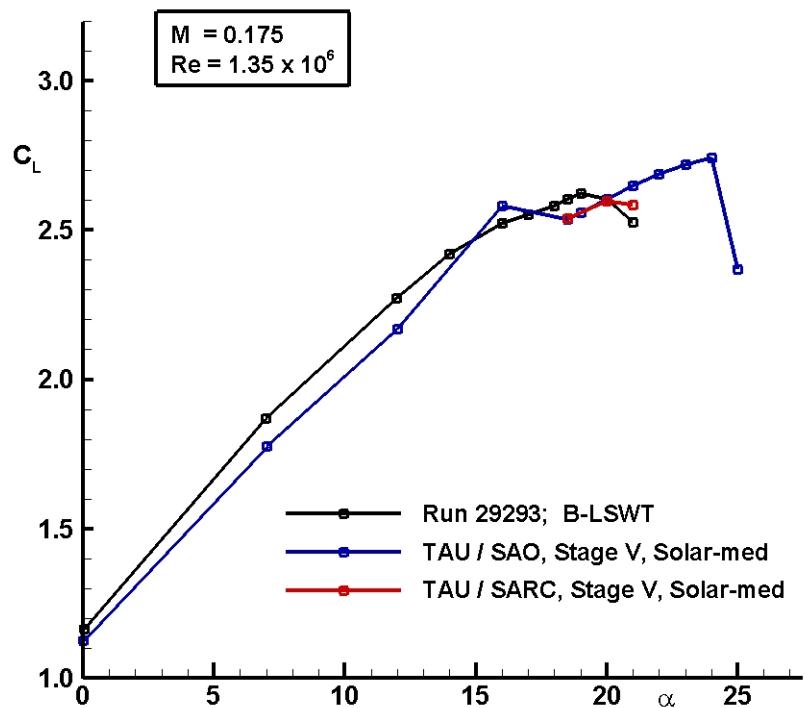
**TAU-SAO / SOLAR**

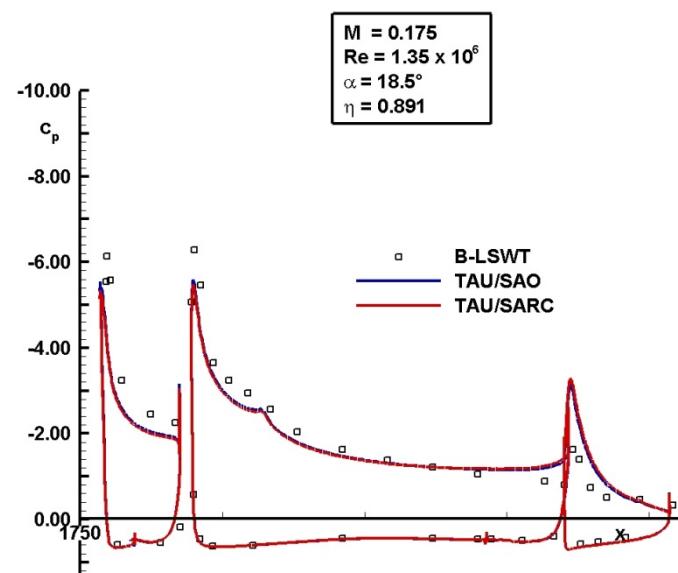
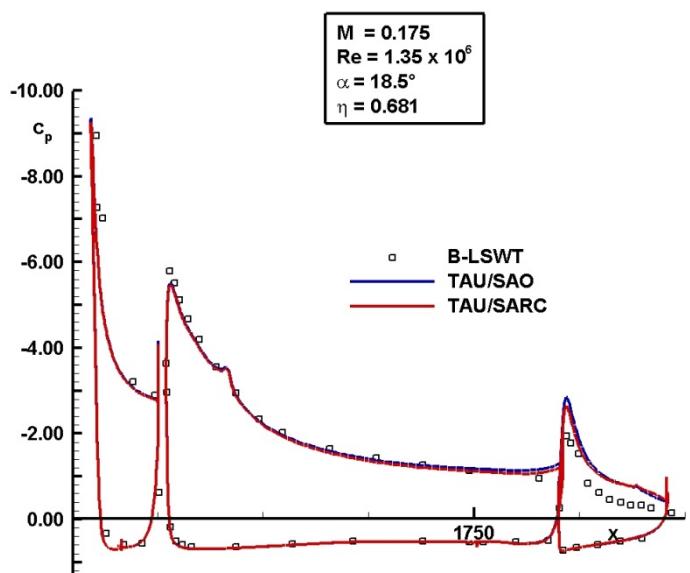
**Turbulence Model Variation SA-RC (in progress)**

**Full Complexity (WB+HLS+PFS+TF+ST+PTB)**

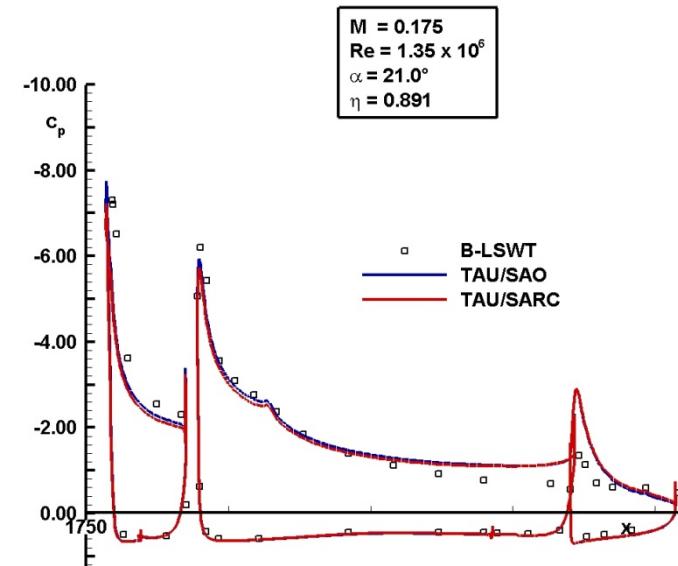
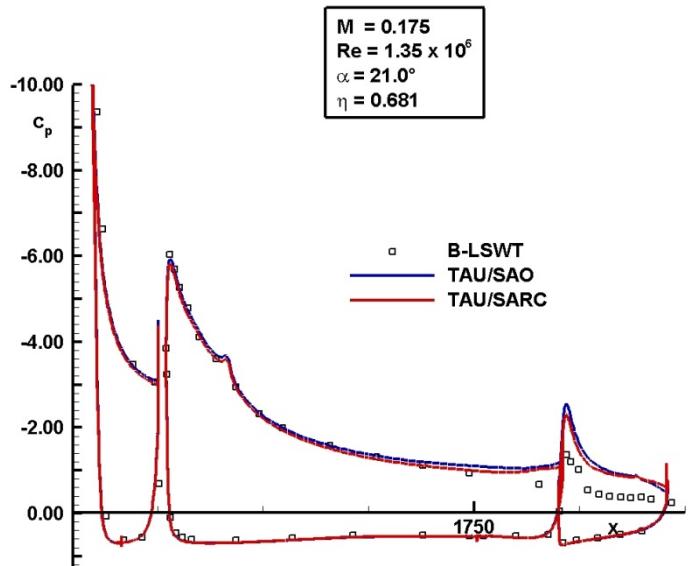
**Low Re No.**

- Lift curve and pitching moment





**$\alpha = 18.5^\circ$**   
**PS6, PS10**



**$\alpha = 21.0^\circ$**   
**PS6, PS10**

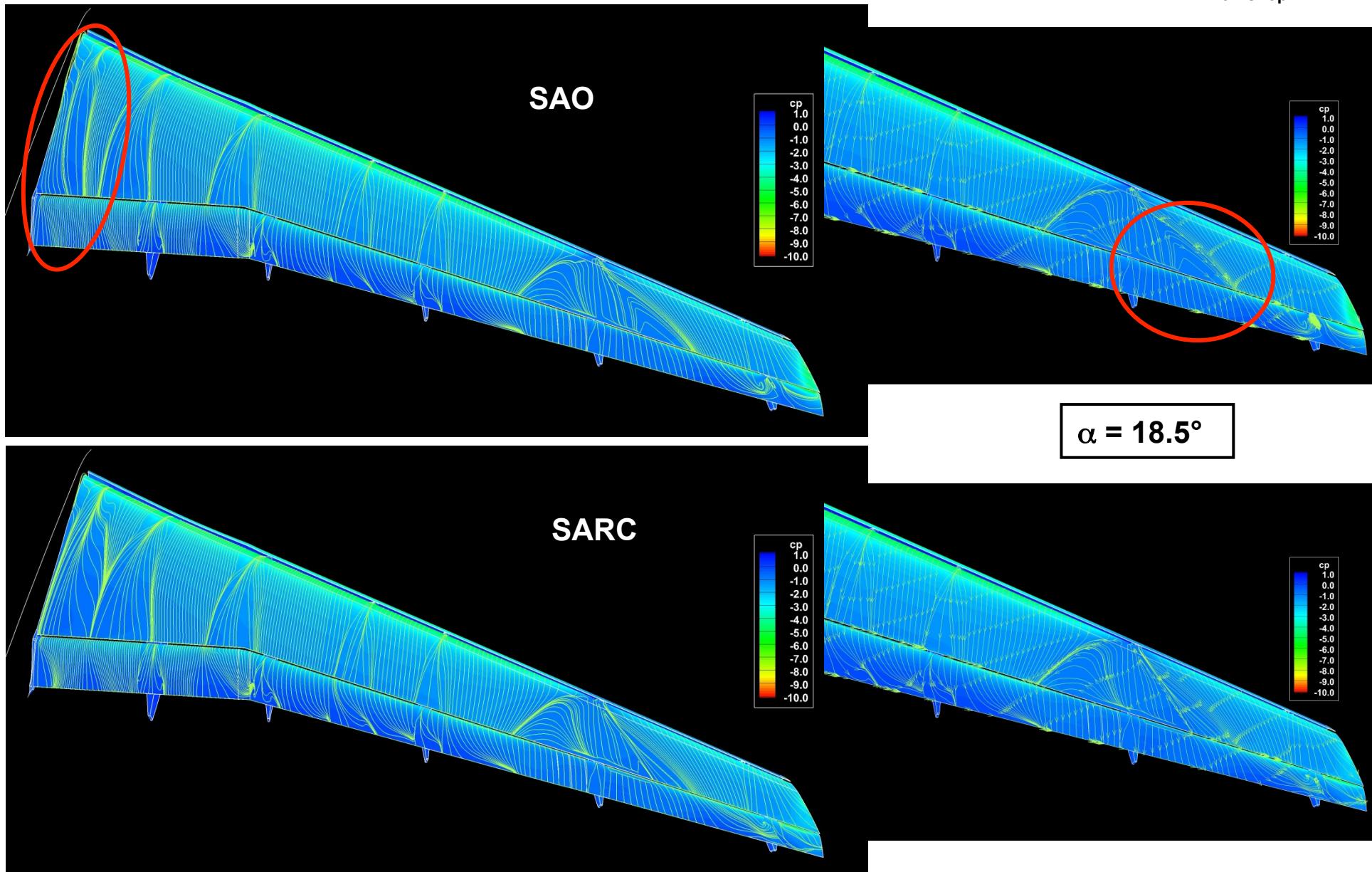


DLR

## TAU/SAO-SARC Solar Grid - Case 3a (low Re-No.)



CFD High Lift Prediction  
Workshop



## Case 1

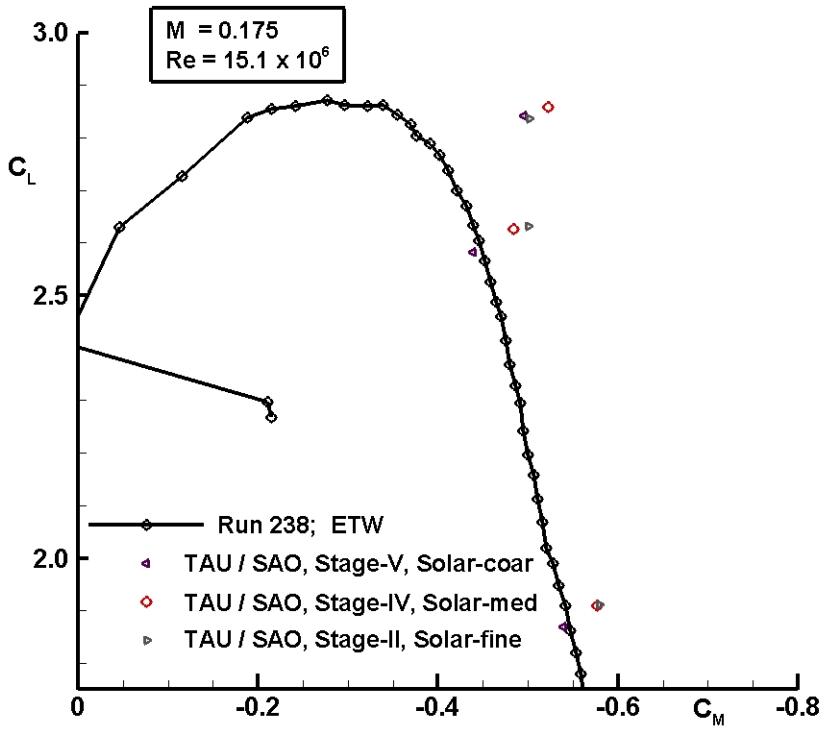
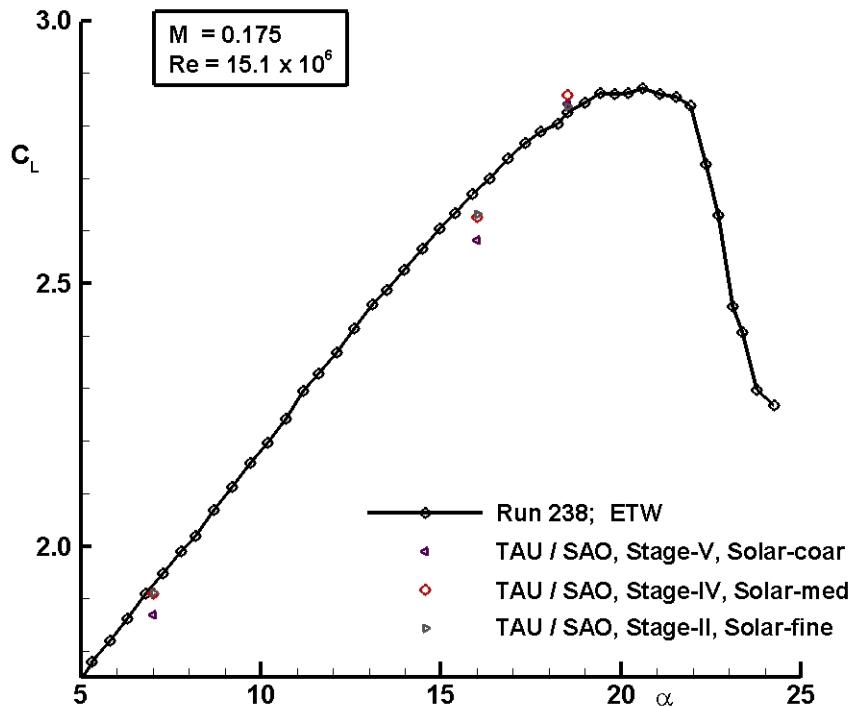
**TAU-SAO / SOLAR**

**Grid Refinement Study**

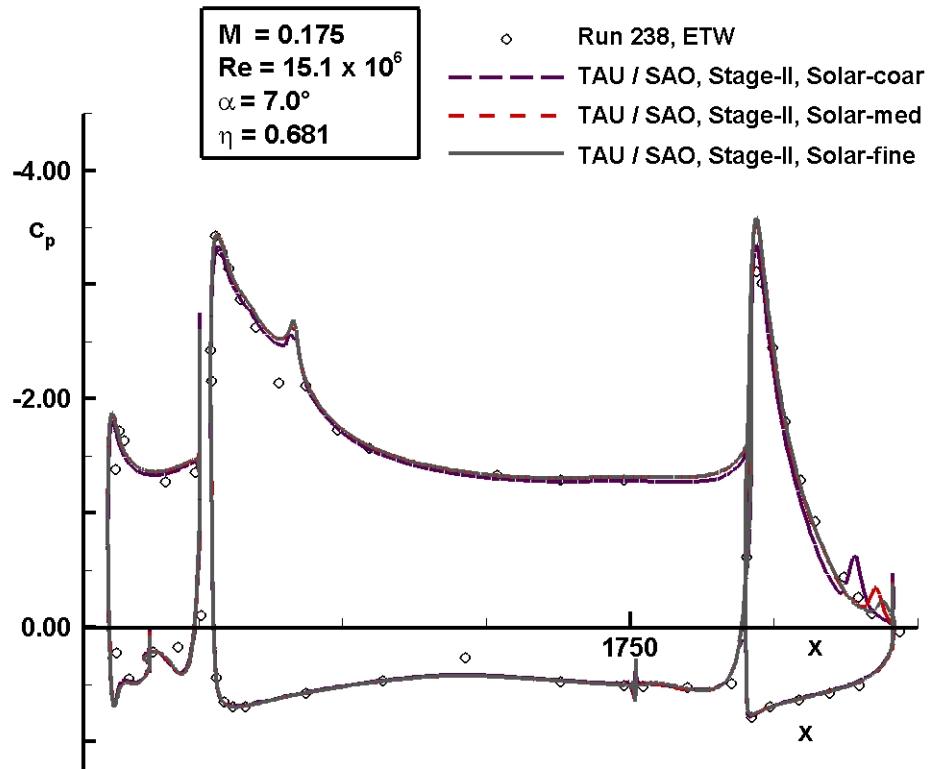
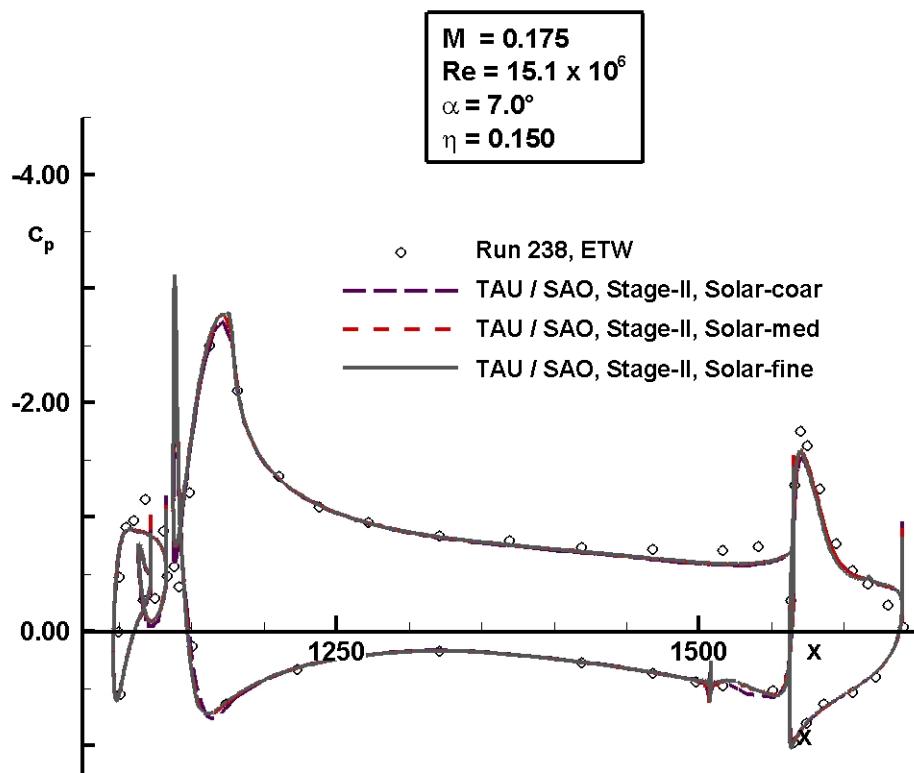
**Simplified Configuration (WB+HLS+PFS)**

**High Re No.**

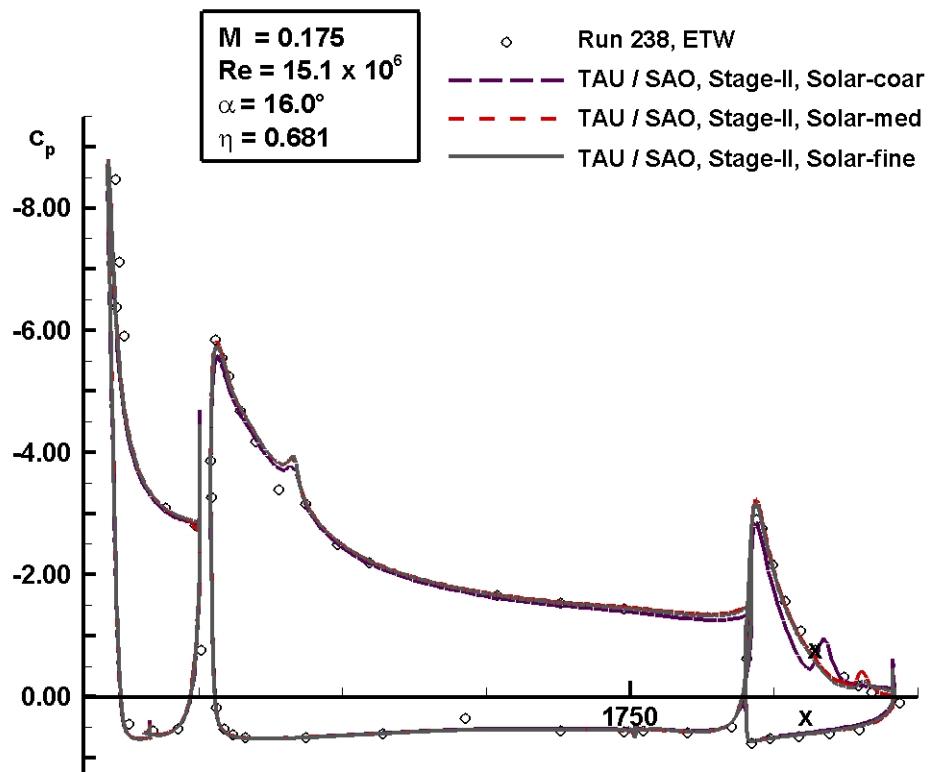
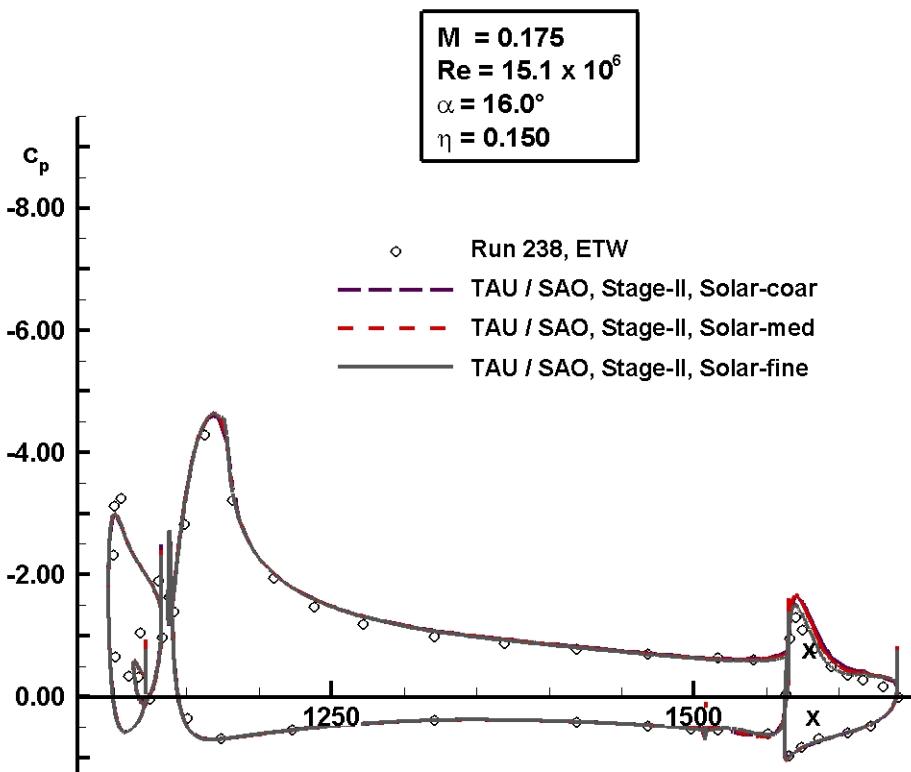
- Lift curve and pitching moment



$\alpha = 7^\circ$   
PS1, PS6

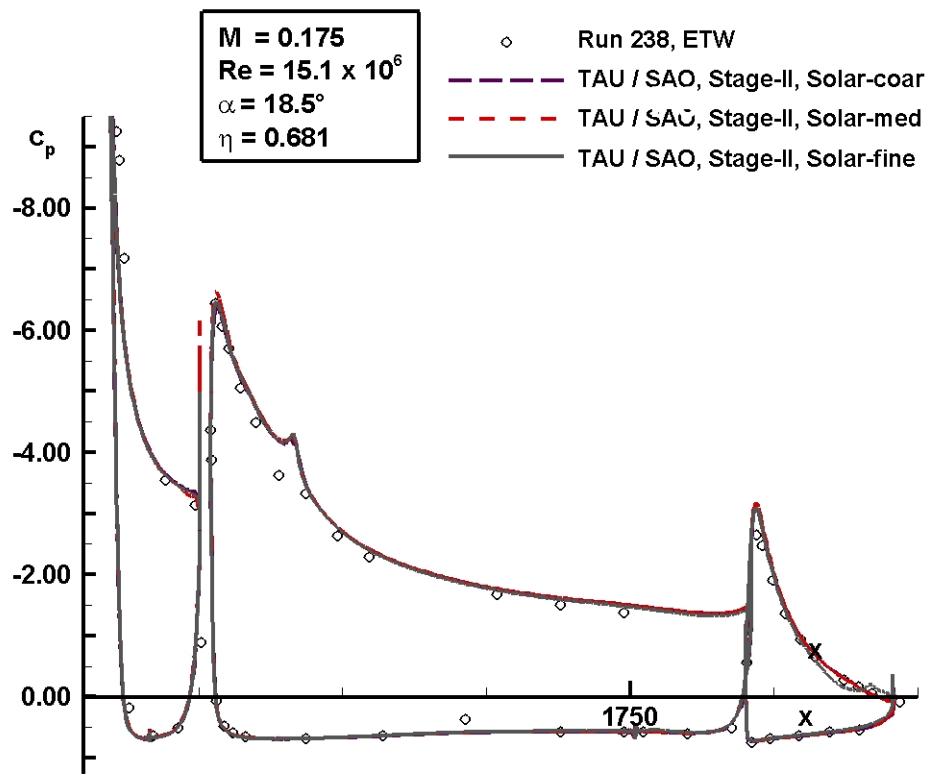
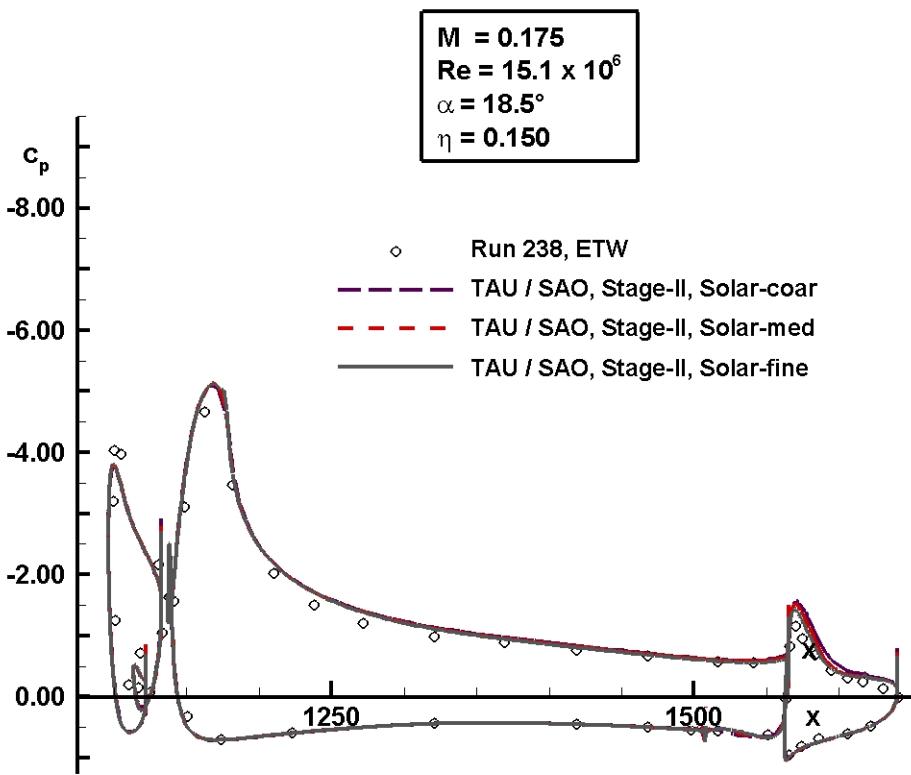


$\alpha = 16^\circ$   
PS1, PS6

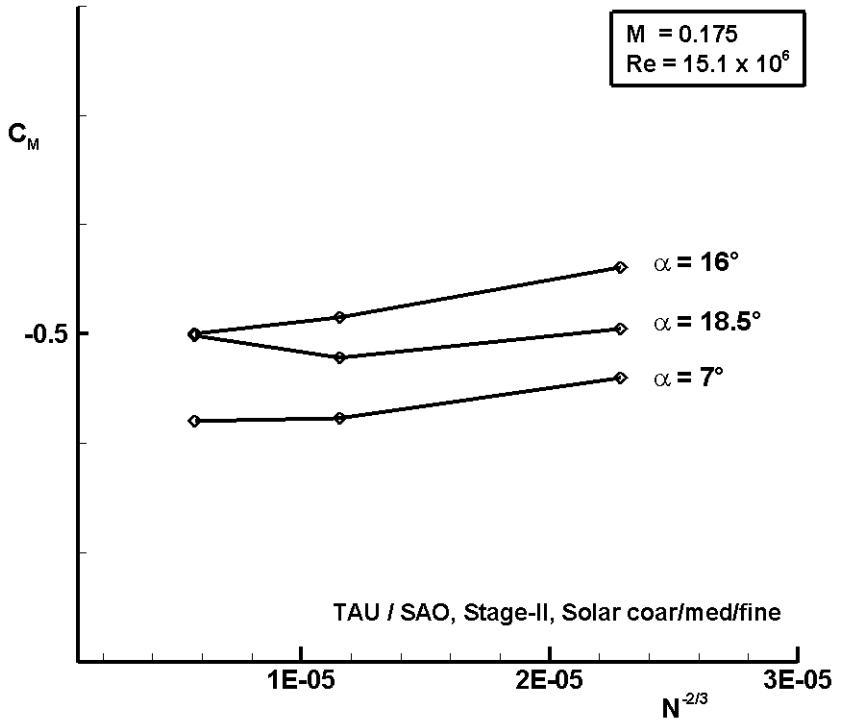
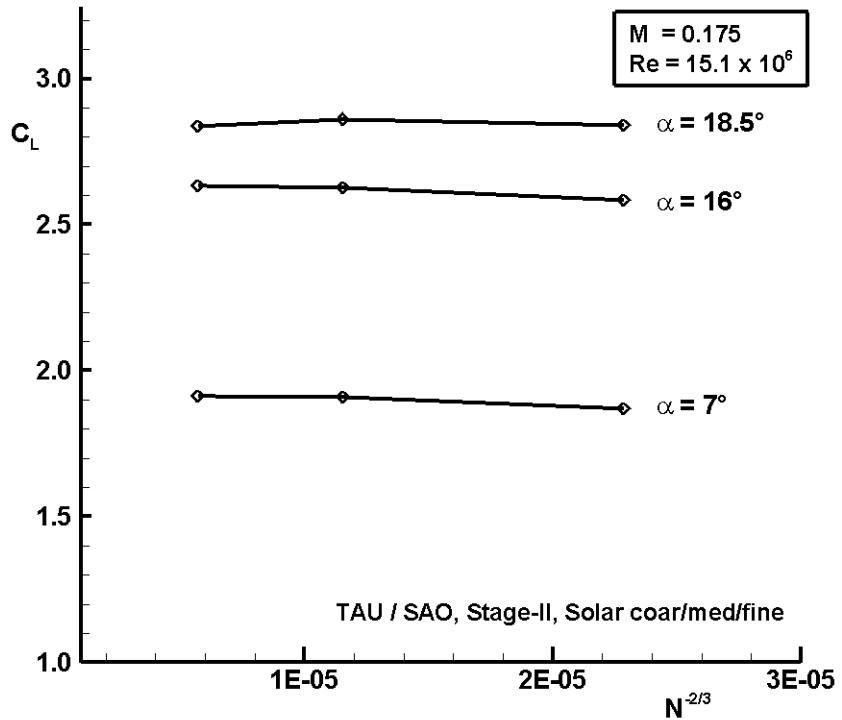


$\alpha = 18.5^\circ$

PS1, PS6



- Lift and pitching moment vs. grid point no.



- RANS computations of the DLR-F11 configuration have been carried out using the DLR TAU code and the SAO turbulence model on hybrid- unstructured grids.
- Hex-dominant grids have been generated with the SOLAR grid generation system for all three complexity stages adapted to low and high Re-No. conditions as well as for a 3-level grid refinement study on the most simplified configuration
- Baseline validation using the SAO model on the most representative configuration reveals:
  - good agreement of  $c_p$ -distributions and forces in the linear lift range
  - singular deviation for  $\alpha = 16^\circ$
  - significant deviations in lift breakdown mechanism and in  $C_{L_{max}}$  and  $\alpha_{max}$
- Reynolds Number Effects are consistently captures, taking into account that the lift breakdown mechanisms (and its simulated deviations) are not affected
- Computed impact of wind tunnel model details on the surface flowfield results in minor effects of the pressure tube bundles and a stronger impact of tracks and FTFs

- Impact of Pressure Tube Bundles is widely limited to the maximum lift regime
  - first order effects are simulated
  - an impact of the singularity at  $\alpha = 16^\circ$  is observed, yet the experimental effects on the lift curve are not consistently reflected
- The rotational correction of the SA model results in a trend to provide an improved agreement to the experimental evidence for low Reynolds number conditions with a large part of the deviations remaining (comp's need to be progressed)
- The grid refinement study shows comparatively small effects on the overall aerodynamic properties, most pronounced at the flap t.e.

- Grid generation
  - Assessment of normal to wall resolution improvements
  - Assessment of track wake resolution
  - Assessment and cross comparison of a different grid system
  
- TAU computations
  - Completion of post  $C_{L_{max}}$  SAO-computations
  - Turbulence model performance assessment for low Re conditions Case 5a (SA-QCR, SSG/LLR- $\omega$ ) with a focus on  $C_{L_{max}}$  range and “16°-singularity”
  - Validation of to simulate and predict transitional effects